## CHAPTER 6

## OPTIMAL BATCH SIZE IN A SINGLE-STAGE IMPERFECT PRODUCTION SYSTEM WITH INSPECTION ERRORS AND OPTIMAL NUMBER OF KANBANS IN A MULTI-STAGE JIT PRODUCTIONDELIVERY SYSTEM WITH REWORK CONSIDERATION


#### Abstract

This chapter depicts the analytical model and numerical computation to determine the optimal batch size in a single-stage production system with rework consideration under different options of raw material ordering and finished goods delivery situations. The model and computational results to determine the optimal number of kanbans in a multi-stage JIT production-delivery system with rework consideration are presented. The managerial implications based on the results are summarized.


### 6.1 Optimal Batch Size in a Single-Stage Imperfect Production System due to Inspection Errors

Ojha et al., (2007) considered a manufacturing system which receives raw material from a supplier, processes it, and delivers it to the customer periodically. They determined the optimal raw material ordering quantity and finished product batch size such that the total cost for the system is minimized. Three different scenarios are considered, viz. (a) a single lot of raw material for multiple lot of finished product and delivery of the product in multiple installments, (b) a single lot of raw material for a multiple lot of finished product and delivery of the product in a single installment, and (c) lot-for-lot and delivery of finished product in single installment. Ben-Daya and Rahim (2003) modeled an imperfect multistage production system considering the (i) effect of inspection errors in screening non-conforming items at various stages and (ii) inspection and restoration of the processes at all stages. They have addressed the following important issues when dealing with imperfect multistage production processes: (i) Nonconforming items must be screened so that they are not passed to subsequent stages, (ii) While screening non-conforming items, good items may be incorrectly rejected and nonconforming items may be incorrectly accepted, and (iii) When the processes shift to an out of control state, production of non-conforming items must be detected.

This research work extends the Ojha et al., (2007) model for the three production - delivery policies incorporating the (i) effect of inspection errors that may be committed while screening defective items and (ii) inspection and restoration of the process as a mean of improving quality. The objective will be to minimize the total system cost in all three policies and to determine the optimal number of inspections and raw material ordering quantity.

The remainder of this section is organized as follows. The necessary notation and assumptions are stated. The determination of optimal batch size incorporating the expected quality cost is provided for all the three production delivery situations. The mathematical model incorporating process inspection and restoration costs in the all the three production delivery systems with defects and inspection errors is also presented. The solution procedure to determine (i) the production batch size and raw material ordering quantity, and (ii) the optimal number of inspections along with the optimal batch size and raw material ordering quantity are described. Numerical examples and sensitivity analysis of the parameters are also presented.

The notations used in this model are defined as follows:
$A_{f} \quad$ setup cost for production (\$ per batch)
$A_{r} \quad$ ordering cost of raw material (\$ per order)
$C_{i} \quad$ cost of inspection (\$ per unit)
$C_{l} \quad$ cost of late delivery (\$ per unit)
C cost of raw material (\$ per unit)
$D_{r} \quad$ demand of raw material (units per cycle)
$D_{f} \quad$ demand rate of the product (units per cycle)
$E_{I} \quad$ probability of incorrectly rejecting a conforming item (type I error)
$E_{2} \quad$ probability of incorrectly accepting a non-conforming item (type II error)
$f_{0} \quad$ conversion factor of raw material $\left(f_{0}=D_{f} / D_{r}=Q_{f} / Q_{r}\right)$
$i \quad$ yearly interest rate
$L \quad$ time between successive shipments $\left(\mathrm{L}=\mathrm{x} / \mathrm{D}_{\mathrm{f}}\right)$
$m \quad$ number of full shipment during production cycle time ( $\mathrm{m}=\mathrm{T} / \mathrm{L}$ )
$n \quad$ number of equivalent batches to a raw material supply
$N_{c} \quad$ number of conforming items in a batch (units)
$N_{n} \quad$ number of non-conforming items in a batch (units)
$N_{r} \quad$ total number of items rejected in a batch (units)
$N_{n c} \quad$ total number of non-conforming items not screened in the inspection (units)
$P \quad$ Production rate (units per year)
$Q_{f} \quad$ production batch size (units)
$Q_{r} \quad$ ordering quantity of raw material (units)
$R(\tau) \quad$ restoration cost, which is a function of detection delay; $R(\tau)=r_{0}+r_{1} \tau$
$s \quad u n i t$ cost of producing a non conforming item
$T$ production cycle time
$t_{1} \quad$ production time of non-defective parts (years)
$t_{2} \quad$ rework time of defective parts (years)
$t_{s}$ setup time
$V \quad$ value added by the production process (\$ per unit)
$x \quad$ shipment quantity to the customer
$\alpha \quad$ percentage of defective items produced when the process is in the out-of control state
$\beta \quad$ fraction of items rejected on inspection of a batch V
$\beta_{1} \quad$ fraction of bad quality items produced in a batch
$\eta \quad$ number of inspections of the process
$\pi_{I} \quad$ cost of incorrectly rejecting a conforming item
$\pi_{2} \quad$ cost of incorrectly accepting a non conforming item
$\tau \quad$ detection delay, i.e. the time elapsed between the occurrence of a shift and the end of the production cycle
$v \quad$ inspection cost of the process

The assumptions used in the models are (Ojha et al., 2007 and Ben-Daya and Rahim, 2003):

1. the production rate is greater than the demand rate.
2. the process starts in the in-control state producing items of perfect quality and the process may shift to the out-of-control state after a time with a known probability distribution. In the out-of-control state, the process starts producing non-conforming items.
3. all the poor quality items can be reworked.
4. the demand is known and deterministic.
5. the product is delivered in equal quantities and at fixed intervals.
6. the product cannot be delivered until the whole lot is produced, reworked, and quality certified.
7. the rework rate is same as the production rate.
8. no defects are produced during rework process.
9. the setup time is negligible.
10. the number of undetected defectives passed onto the customer is negligible.

### 6.1.1 Model formulation for optimal batch size and number of inspections in a single-stage imperfect production system incorporating process inspection and restoration

The models formulated for optimal batch size and number of inspections in a single-stage imperfect production system are: (i) single purchase multiple delivery (SPMD) with inspection errors, (ii) single purchase multiple delivery (SPMD) with process inspection and restoration, (iii) single purchase single delivery (SPSD) with inspection errors, (iv) single purchase single delivery (SPSD) with inspection and restoration, (v) lot-for-lot (LFL) with inspection errors, (vi) lot-for-lot (LFL) with process inspection and restoration.

### 6.1.1.1 Single purchase multiple delivery (SPMD) with inspection errors

The SPMD policy is adopted when the customer requires the delivery to be made in small installments. Each batch of finished goods is inspected so that the non-conforming items can be removed from the batch and reworked. Non-conforming items at each level are removed and not passed to the following stage. The reworked items are again added to the finished goods lot for final dispatch.

Fig. 6.1 shows the consumption of raw material inventory, build-up of the finished goods inventory with the start of each production cycle, production of the non-defective end product, and rework of the defective items (Ojha et al., 2007). The raw material is consumed by the end of $\mathrm{n}^{\text {th }}$ cycle. The finished goods inventory starts to build up with start of each production cycle, and the production of non-defective end product occurs for at time $t_{1}$ at the rate of $P(1-\beta)$. After the production uptime $t_{1}$, the rework begins at rate $P$, continues for a time $t_{2}$, and reaches a maximum inventory of $\mathrm{Q}_{\mathrm{f}}$ when all items are reworked. The delivery of the finished goods is
made in small equal installments of $x$ at an equal interval of time L. Each supply decreases the finished product inventory by x and the finished product inventory is consumed after m deliveries.


Fig. 6.1 Single purchase multiple delivery (SPMD)

The average raw material inventory is given by
$\bar{I}_{r}=\frac{1}{T}\left[\left(\frac{1}{2} Q_{r} t_{1}+Q_{r} T\right)+\left(\frac{1}{2} Q_{r} t_{1}+Q_{r} 2 T\right)+\ldots \ldots \ldots \ldots .\left(\frac{1}{2} Q_{r} t_{1}+Q_{r}(n-1) T\right)\right]=$
$\frac{1}{T}\left[\frac{1}{2} n Q_{r} t_{1}+\frac{1}{2} Q_{r} n(n-1) T\right]=\frac{Q_{f}}{T f_{0}}\left[\frac{D_{f}}{P}+n-1\right]$
The inventory carrying cost of raw material is
$I_{R}=\frac{i C Q_{f}}{2 f_{0}}\left[\frac{D_{f}}{P}+n-1\right]$
The ordering cost of one lot of raw material is
$A_{R}=\frac{D_{r}}{n Q_{r}} A_{r}=\frac{D_{f}}{n Q_{f}} A_{r}$
The average finished product inventory which is delivered in small equal installments x is
$\bar{I}=\frac{Q_{f} D_{f}}{2 P}[1+\beta(1-\beta)]+\frac{1}{m L}[x(m-1) L+x(m-2) L+\ldots \ldots .+x L]=$
$\frac{Q_{f} D_{f}}{2 P}[1+\beta(1-\beta)]+\frac{1}{2} x(m-1)$
The total finished goods inventory carrying cost is
$I_{F}=i(C+V)\left[\frac{Q_{f} D_{f}}{2 P}[1+\beta(1-\beta)]+\frac{1}{2} x(m-1)\right]$
The processing cost of the raw material per batch quantity $\mathrm{Q}_{\mathrm{f}}$ processed in every cycle is $\mathrm{VQ}_{\mathrm{f}}$. The total processing cost over the year is

$$
\begin{equation*}
K_{F}=\left(V Q_{f}\right) \frac{D_{f}}{Q_{f}}=V D_{f} \tag{6.6}
\end{equation*}
$$

The proportion of the defective products in a cycle is $\beta$. The amount of the defective items produced in a cycle is $\beta \mathrm{Q}_{\mathrm{f}}$. The rework processing cost of the defectives per year is
$K_{R E}=\left(V \beta Q_{f}\right) \frac{D_{f}}{Q_{f}}=V \beta D_{f}$
The inventory of defective items produced per cycle is carried over for $t_{2}$ time. The rework inventory carrying cost is

$$
\begin{equation*}
I_{R E}=\frac{\beta Q_{f}}{2} i(C+V) \frac{D_{f}}{P}+\frac{\beta Q_{f}}{2} i(C+2 V) \frac{\beta D_{f}}{P}=\frac{i \beta Q_{f} D_{f}}{2 P}(C+V+\beta C+2 \beta V) \tag{6.8}
\end{equation*}
$$

The total inspection cost per cycle is

$$
\begin{equation*}
C_{I}=Q_{f} C_{i} \tag{6.9}
\end{equation*}
$$

The finished material are delivered late in each cycle by time $t_{2}$. The total late delivery per cycle is

$$
\begin{equation*}
C_{L}=t_{2} C_{l}=\frac{\beta Q_{f}}{P} C_{l} \tag{6.10}
\end{equation*}
$$

Also the finished products are not produced in time $t_{2}$. The cost per cycle to miss out an opportunity of producing more of the finished products is

$$
\begin{equation*}
C_{L P}=V \beta Q_{f} \tag{6.11}
\end{equation*}
$$

The total cost is the sum of inventory carrying cost of raw material, ordering cost of raw material, setup cost, finished goods inventory carrying cost, processing cost, reworking processing cost of defective items, rework inventory carrying cost, inspection cost, late delivery cost and lost production cost is (Ojha et al., 2007):

$$
\begin{align*}
& T C(m, n)=\frac{i C Q_{f}}{2 f_{0}}\left[\frac{D_{f}}{P}+n-1\right]+\frac{D_{f}}{Q_{f}}\left(\frac{A_{r}}{n}+A_{f}\right)+i(C+V)\left[\frac{Q_{f} D_{f}}{2 P}[1+\beta(1-\beta)]+\frac{1}{2} x(m-1)\right]+ \\
& V D_{f}(1+\beta)+\frac{i \beta Q_{f} D_{f}}{2 P}(C+V+\beta C+2 \beta V)+Q_{f}\left(C_{i}+\frac{\beta C_{l}}{P}+V \beta\right) \tag{6.12}
\end{align*}
$$

A lot of $\mathrm{Q}_{\mathrm{f}}$ conforming products are required for the final product. The number of items rejected from a lot is the sum of incorrectly rejecting a confirming item and correctly rejecting a nonconforming item. The conforming items in a batch are $\left(Q_{f}-N_{n}\right)$ and the number of nonconforming items in a batch are $\mathrm{N}_{\mathrm{n}}$ are shown in Fig. 6.2. The number of incorrectly rejected conforming items are $\left(Q_{f}-N_{n}\right) E_{1}$ and the number of correctly accepted conforming items are $\left(Q_{f}-N_{n}\right)\left(1-E_{1}\right)$. The correctly rejected non-conforming items are $N_{n}\left(1-E_{2}\right)$ and the incorrectly accepted non-conforming items are $N_{n} E_{2}$.


Fig. 6.2 Effect of inspection errors

Thus, the total number of items rejected in a batch is
$N_{r}=N_{n}\left(1-E_{2}\right)+\left(Q_{f}-N_{n}\right) E_{1}$
Therefore the effective rejection rate is $\beta=N_{r} / Q_{f}$.
The expected number of non-conforming items produced at any stage once the corresponding process shifts to an out of control state is given by (Ben-Daya and Rahim, 2003)

$$
\begin{equation*}
N_{n}=\int_{0}^{t_{1}} \alpha P\left(t_{1}-t\right) \frac{e^{-t / \theta}}{\theta} d t=\alpha P\left(t_{1}-\theta+\theta_{1} e^{-t_{1} / \theta}\right) \tag{6.14}
\end{equation*}
$$

Using the approximation $e^{-t_{1} / \theta} \approx 1-t_{1} / \theta+0.5\left(t_{1} / \theta\right)^{2}$ by Mc Laurin series (Moon et al., 2002) and substituting in Eq. (6.14) the number of non-conforming items in a batch is

$$
\begin{equation*}
N_{n}=\frac{\alpha P t_{1}^{2}}{2 \theta}=\frac{\alpha Q_{f}^{2}}{2 P \theta} \tag{6.15}
\end{equation*}
$$

where $t_{1}=Q_{f} / P$
From Eqs. (6.13) and (6.15), the effective rejection rate is
$\beta=\frac{N_{r}}{Q_{f}}=\frac{\alpha Q_{f}}{2 P \theta}\left(1-E_{2}\right)+\left(1-\frac{\alpha Q_{f}}{2 P \theta}\right) E_{1}$
The expected quality costs per unit time due to non-conforming items and inspection errors are given by (Ben-Daya and Rahim, 2003)

$$
\begin{align*}
& K_{Q C}=\frac{D_{f}}{Q_{f}}\left(s N_{n}\left(1-E_{2}\right)+\pi_{1}\left(Q_{f}-N_{n}\right) E_{1}+\pi_{2} N_{n} E_{2}\right)=  \tag{6.17}\\
& D_{f}\left(\pi_{1} E_{1}+\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha Q_{f}}{2 P \theta}\right)
\end{align*}
$$

As $Q_{f}=m x$, the expected total cost from Eqs. (6.12), (6.16) and (6.17) is written as

$$
\begin{align*}
& T C(m, n)=\frac{i C m x}{2 f_{0}}\left[\frac{D_{f}}{P}+n-1\right]+\frac{D_{f}}{m x}\left(\frac{A_{r}}{n}+A_{f}\right)+i(C+V)\left[\frac{m x D_{f}}{2 P}[1+\beta(1-\beta)]+\frac{1}{2} x(m-1)\right]+ \\
& V D_{f}(1+\beta)+D_{f}\left(\pi_{1} E_{1}+\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha m x}{2 P \theta}\right)+ \\
& \frac{i \beta m x D_{f}}{2 P}(C+V+\beta C+2 \beta V)+m x\left(C_{i}+\frac{\beta C_{l}}{P}+V \beta\right) \tag{6.18}
\end{align*}
$$

The total cost function is convex in both n and m . Optimal values of $n$ and $m$ are found by differentiating the total cost function with respect to n and m , and equating the resulting expression to zero. Differentiating Eq. (6.18) with respect to $n$ and equating the resulting the expression to zero, the optimal value of $n$ is obtained as;
$n^{*}=\frac{1}{m x} \sqrt{\frac{2 f_{0} D_{f} A_{r}}{i C}}$
Similarly, differentiating the Eq. (6.18) with respect to $m$ and equating the resulting expression to zero yields;

$$
\begin{align*}
& \frac{\partial T C(m, n)}{\partial m}=\frac{i C x}{2 f_{0}}\left[\frac{D_{f}}{P}+n-1\right]-\frac{D_{f}}{m^{2} x}\left(\frac{A_{r}}{n}+A_{f}\right)+ \\
& i(C+V)\left[\frac{x D_{f}}{2 P}[1+\beta(1-\beta)]+\frac{m x D_{f}}{2 P} \frac{d \beta}{d m}(1-2 \beta)+\frac{1}{2} x\right]+ \\
& V D_{f} \frac{d \beta}{d m}+D_{f}\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha x}{2 P \theta}+\frac{i x D_{f} \beta}{2 P}(C+V+\beta C+2 \beta V)+ \\
& \frac{i m x D_{f}}{2 P} \frac{d \beta}{d m}(C+V+2 \beta C+4 \beta V)+x\left(C_{i}+\frac{\beta C_{l}}{P}+V \beta\right)+m x \frac{d \beta}{d m}\left(\frac{C_{l}}{P}+V\right)=0 \tag{6.20}
\end{align*}
$$

where $\frac{d \beta}{d m}=\frac{\alpha x}{2 P \theta}\left(1-E_{1}-E_{2}\right)$
The solution algorithm is as follows:

Step 1: Using the values of $n *$ from Eq. (6.19) and $\beta$ from Eq. (6.16), solve Eq. (6.20) using Newton-Raphson iterative procedure till the convergence of $m^{*}$ and $n^{*}$ are obtained.
The convergence criteria for algorithm is: $\left|\frac{\frac{\partial T C(m, n)}{\partial m}}{\frac{\partial^{2} T C(m, n)}{\partial m^{2}}}\right| \leq 10^{-3}$

The convergence criteria for algorithm is: $\left|\frac{\frac{\partial T C(m, n, \eta)}{\partial m}}{\frac{\partial^{2} T C(m, n, \eta)}{\partial m^{2}}}\right| \leq 10^{-3}$
The convergence criteria for algorithm is: $\left|\frac{\frac{\partial T C(m, n, \eta)}{\partial \eta}}{\frac{\partial^{2} T C(m, n, \eta)}{\partial \eta^{2}}}\right| \leq 10^{-3}$

Step 2:
(i) If $\mathrm{n}^{*}<1$ then choose $n^{*}=1$.
(a) If $\mathrm{m}^{*}<1$, then choose $m^{*}=1$. Determine $\beta^{*}$ (1) from Eq. (6.16). Compute $T C^{*}(1,1)$ from Eq. (6.18).
(b) If $\mathrm{m}^{*}>1$, then for $J_{m}{ }^{*}<m^{*}<J_{m}{ }^{*}+1\left(J_{m}\right.$ is a positive integer), determine $\beta^{*}\left(J_{m}{ }^{*}\right)$ and $\beta^{*}\left(J_{m} *+1\right)$ from Eq. (6.16). Compute $T C *\left(1, J_{m} *\right)$ and $T C^{*}\left(1, J_{m} *+1\right)$ from Eq. (6.18) and choose the one with smaller value as the optimal solution.
(ii) If $n^{*}>1$, then choose $J_{n}{ }^{*}<n^{*}<J_{n}{ }^{*}+1$ (where $J_{n}$ is a positive integer).
(a) If $\mathrm{m}^{*}<1$, then choose $m^{*}=1$. Determine $\beta^{*}$ (1) from Eq. (6.16). Compute $T C^{*}\left(J_{n}{ }^{*}, l\right)$ and $T C^{*}\left(J_{n} *+1, l\right)$ from Eq. (6.18) and choose the one with smaller value as the optimal solution.
(b) If $\mathrm{m}^{*}>1$, and $J_{m}{ }^{*}<m^{*}<J_{m}{ }^{*}+1$ (where $J_{m}$ is a positive integer), determine $\beta^{*}$ $\left(J_{m}{ }^{*}\right)$ and $\beta^{*}\left(J_{m} *+1\right)$ from Eq. (6.16). Compute $T C *\left(J_{n} *, J_{m} *\right), T C *\left(J_{n} *+1, J_{m} *\right)$, $T C^{*}\left(J_{n}{ }^{*}, J_{m}{ }^{*}+1\right)$ and $T C *\left(J_{n} *+1, J_{m} *+1\right)$ from Eq. (6.18) and choose the one with smaller value as the optimal solution.

### 6.1.1.2 Single purchase multiple delivery (SPMD) with process inspection and restoration

Production process is inspected at regular intervals during a production run and if it is found to be out of control, necessary actions are taken to restore it to the in control state (Ben-Daya and Rahim, 2003). Lee and Rosenblatt (1989) determined the production and inspection schedules for a system in which cost of maintenance depends on detection delay, i.e., the number of periods in the out-of-control state. The optimum maintenance schedule is determined as a function of the cost of defective items, the cost of restoration and the mean time until the system is out of control. Scheduling inspections at regular intervals has been shown to be optimal in cases of exponentially distributed time to shift to the out of control state.
The expected number of non conforming items, $\mathrm{N}_{\mathrm{i} \eta}$ produced during inspection is given by

$$
\begin{equation*}
N_{i \eta}=\int_{0}^{t_{1} / \eta} \alpha P\left(\frac{t_{1}}{\eta}-t\right) \frac{e^{-t / \theta}}{\theta} d t=\alpha P\left(\frac{t_{1}}{\eta}-\theta+\theta e^{-t_{1} /(\eta \theta)}\right) \approx \frac{\alpha P}{2}\left(\frac{t_{1}}{\eta \theta}\right)^{2}=\frac{\alpha Q_{f}^{2}}{2 \eta^{2} P \theta} \tag{6.21}
\end{equation*}
$$

The total expected number of non conforming items $\mathrm{N}_{\mathrm{i}}$, produced during a complete production run of the process is

$$
\begin{equation*}
N_{i}=\eta N_{i \eta}=\frac{\alpha Q_{f}^{2}}{2 \eta P \theta} \tag{6.22}
\end{equation*}
$$

Thus, the effective rejection rate is

$$
\begin{equation*}
\beta_{i}=\frac{N_{i}}{Q_{f}}=\frac{\alpha Q_{f}}{2 \eta P \theta}\left(1-E_{2}\right)+\left(1-\frac{\alpha Q_{f}}{2 \eta P \theta}\right) E_{1} \tag{6.23}
\end{equation*}
$$

Hence the expected quality costs per unit time due to non-conforming items and inspection errors are given by

$$
\begin{equation*}
K_{Q C I}=\frac{D_{f}}{Q_{f}}\left(s N_{i}\left(1-E_{2}\right)+\pi_{1}\left(Q_{f}-N_{i}\right) E_{1}+\pi_{2} N_{i} E_{2}\right)=D_{f}\left(\pi_{1} E_{1}+\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha Q_{f}}{2 \eta P \theta}\right) \tag{6.24}
\end{equation*}
$$

The inspection cost is given by

$$
\begin{equation*}
K_{I C}=\frac{D_{f}}{Q_{f}} \eta v \tag{6.25}
\end{equation*}
$$

It is assumed that the restoration cost depends on the detection delay, then the expected restoration cost during the inspection of the process is given by

$$
\begin{align*}
& K_{R C \eta}=\int_{0}^{t_{1} / \eta}\left[r_{0}+r_{1}\left(\frac{t_{1}}{\eta}-t\right)\right] \frac{e^{-t / \theta}}{\theta} d t=\left(r_{0}+r_{1} \frac{t_{1}}{\eta}-r_{1} \theta\right)+\left(r_{1} \theta-r_{0}\right) e^{-t_{1} /(\eta \theta)}  \tag{6.26}\\
& =\left(r_{1} \theta-r_{0}\right) \frac{t_{1}^{2}}{2 \eta^{2} \theta^{2}}+\frac{r_{0} t_{1}}{\eta \theta}=\left(r_{1} \theta-r_{0}\right) \frac{Q_{f}^{2}}{2 \eta^{2} P^{2} \theta^{2}}+\frac{r_{0} Q_{f}}{\eta P \theta}
\end{align*}
$$

The expected restoration cost for the complete system is

$$
\begin{equation*}
K_{R C}=\frac{D_{f}}{Q_{f}}\left(\eta K_{R C \eta}\right)=\frac{Q_{f} D_{f}}{2 \eta P^{2} \theta^{2}}\left(r_{1} \theta-r_{0}\right)+\frac{D_{f} r_{0}}{P \theta} \tag{6.27}
\end{equation*}
$$

The expected total cost including inspection and restoration from Eqs. (6.12), (6.23), (6.24), (6.25) and (6.27) is written as
$T C(m, n, \eta)=\frac{i C m x}{2 f_{0}}\left[\frac{D_{f}}{P}+n-1\right]+\frac{D_{f}}{m x}\left(\frac{A_{r}}{n}+A_{f}\right)+i(C+V)\left[\frac{m x D_{f}}{2 P}\left[1+\beta_{i}\left(1-\beta_{i}\right)\right]+\frac{1}{2} x(m-1)\right]+$
$V D_{f}\left(1+\beta_{i}\right)+D_{f}\left(\pi_{1} E_{1}+\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha m x}{2 \eta P \theta}\right)+\frac{i \beta_{i} m x D_{f}}{2 P}\left(C+V+\beta_{i} C+2 \beta_{i} V\right)+$ $m x\left(C_{i}+\frac{\beta_{i} C_{l}}{P}+V \beta_{i}\right)+\frac{D_{f}}{m x} \eta_{v}+\frac{m x D_{f}}{2 \eta P^{2} \theta^{2}}\left(r_{1} \theta-r_{0}\right)+\frac{D_{f} r_{0}}{P \theta}$

Differentiating Eq. (6.18) with respect to $n$ and equating the resulting the expression to zero, the optimal value of $n$ is shown in Eq. (6.19).

Differentiating the Eq. (6.28) with respect to $m$ and equating the resulting expression to zero yields;

$$
\begin{align*}
& \frac{\partial T C(m, n, \eta)}{\partial m}=\frac{i C x}{2 f_{0}}\left[\frac{D_{f}}{P}+n-1\right]-\frac{D_{f}}{m^{2} x}\left(\frac{A_{r}}{n}+A_{f}\right)+i(C+V)\left[\frac{x D_{f}}{2 P}\left[1+\beta_{i}\left(1-\beta_{i}\right)\right]+\frac{1}{2} x\right]+ \\
& i(C+V) \frac{m x D_{f}}{2 P}\left(\frac{\partial \beta_{i}}{\partial m}-2 \beta_{i} \frac{\partial \beta_{i}}{\partial m}\right)+V D_{f} \frac{\partial \beta_{i}}{\partial m}+D_{f}\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha x}{2 \eta P \theta}+ \\
& \frac{i x D_{f}}{2 P}\left(\beta_{i} C+\beta_{i} V+\beta_{i}^{2} C+2 \beta_{i}^{2} V\right)+\frac{i m x D_{f}}{2 P}\left(\frac{\partial \beta_{i}}{\partial m} C+\frac{\partial \beta_{i}}{\partial m} V+2 \beta_{i} \frac{\partial \beta_{i}}{\partial m} C+4 \beta_{i} \frac{\partial \beta_{i}}{\partial m} V\right)+ \\
& x\left(C_{i}+\frac{\beta_{i} C_{l}}{P}+V \beta_{i}\right)+m x\left(\frac{C_{l}}{P} \frac{\partial \beta_{i}}{\partial m}+V \frac{\partial \beta_{i}}{\partial m}\right)-\frac{D_{f}}{m^{2} x} \eta v+\frac{x D_{f}}{2 \eta P^{2} \theta^{2}}\left(r_{1} \theta-r_{0}\right)=0 \tag{6.29}
\end{align*}
$$

where $\frac{\partial \beta_{i}}{\partial m}=\frac{\alpha x}{2 \eta P \theta}\left(1-E_{1}-E_{2}\right)$

Differentiating the Eq. (6.28) with respect to $\eta$ and equating the resulting expression to zero yields;

$$
\begin{align*}
& \frac{\partial T C(m, n, \eta)}{\partial \eta}=i(C+V) \frac{m x D_{f}}{2 P} \frac{\partial \beta_{i}}{\partial \eta}\left(1-2 \beta_{i}\right)+V D_{f} \frac{\partial \beta_{i}}{\partial \eta}-D_{f}\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha m x}{2 \eta^{2} P \theta}+ \\
& \frac{i m x D_{f}}{2 P} \frac{\partial \beta_{i}}{\partial \eta}\left[(C+V)+2 \beta_{i}(C+2 V)\right]+m x \frac{\partial \beta_{i}}{\partial \eta}\left(\frac{C_{l}}{P}+V\right)+\frac{D_{f}}{m x} v-\frac{m x D_{f}}{2 \eta^{2} P^{2} \theta^{2}}\left(r_{1} \theta-r_{0}\right)=0 \tag{6.30}
\end{align*}
$$

where $\frac{\partial \beta_{i}}{\partial \eta}=-\frac{\alpha m x}{2 \eta^{2} P \theta}\left(1-E_{1}-E_{2}\right)$

The solution algorithm for this model is as follows:
Step 1: Using the values of $n^{*}$ from Eq. (6.19) and $\beta$ from Eq. (6.23), solve Eq. (6.29) using Newton-Raphson iterative procedure till the convergence of $m^{*}$ and $n^{*}$ are obtained.
Step 2: Repeat the step 1 using the current value of $\eta^{*}$ obtained by solving Eq. (6.30) using Newton-Raphson iterative procedure, till the convergence of $\eta^{*}$ is obtained.

Step 3:
(i) If $\eta^{*}<1$ then choose $\eta^{*}=1$.
(a) If $\mathrm{n}^{*}<1$ then choose $n^{*}=1$.

1. If $m^{*}<1$, then choose $m^{*}=1$. Determine $\beta^{*}$ (1) from Eq. (6.23). Compute $T C^{*}(1,1,1)$ from Eq. (6.28).
2. If $\mathrm{m} *>1$, then for $J_{m}{ }^{*}<m^{*}<J_{m}{ }^{*}+l\left(J_{m}\right.$ is a positive integer), determine $\beta^{*}\left(J_{m}{ }^{*}\right)$ and $\beta^{*}\left(J_{m}{ }^{*}+1\right)$ from Eq. (6.23). Compute $T C^{*}\left(1, J_{m}{ }^{*}, 1\right)$ and $T C *\left(1, J_{m} *+1,1\right)$ from Eq. (6.28) and choose the one with smaller value as the optimal solution.
(b) If $n^{*}>1$, then choose $J_{n}^{*}<n^{*}<J_{n} *+1$ (where $J_{n}$ is a positive integer).
3. If $\mathrm{m}^{*}<1$, then choose $m^{*}=1$. Determine $\beta^{*}$ (1) from Eq. (6.23). Compute $T C^{*}\left(J_{n}{ }^{*}, 1,1\right)$ and $T C^{*}\left(J_{n} *+1,1,1\right)$ from Eq. (6.28) and choose the one with smaller value as the optimal solution.
4. If $\mathrm{m}^{*}>1$, and $J_{m}{ }^{*}<m^{*}<J_{m}{ }^{*}+1$ (where $J_{m}$ is a positive integer), determine $\beta^{*}\left(J_{m}{ }^{*}\right)$ and $\beta^{*}\left(J_{m}{ }^{*}+1\right)$ from Eq. (6.23). Compute $T C^{*}\left(J_{n}{ }^{*}\right.$, $\left.J_{m}{ }^{*}, l\right), T C^{*}\left(J_{n} *+1, J_{m} *, l\right), T C^{*}\left(J_{n}{ }^{*}, J_{m} *+1,1\right)$ and $T C^{*}\left(J_{n} *+1, J_{m}{ }^{*}+1,1\right)$
from Eq. (6.28) and choose the one with smaller value as the optimal solution.
(ii) If $\eta^{*}>1$ then choose $J_{\eta}^{*}<n^{*}<J_{\eta}{ }^{*}+1$ (where $J_{\eta}$ is a positive integer)
(a) If $\mathrm{n}^{*}<1$ then choose $n^{*}=1$.
5. If $m^{*}<1$, then choose $m^{*}=1$. Determine $\beta^{*}$ (1) from Eq. (6.23). Compute $T C^{*}\left(1,1, J_{\eta}{ }^{*}\right)$ and $T C^{*}\left(1,1, J_{\eta}{ }^{*}+1\right)$ from Eq. (6.28) and choose the one with smaller value as the optimal solution.
6. If $\mathrm{m}^{*}>1$, then for $J_{m}{ }^{*}<m^{*}<J_{m}{ }^{*}+1$ ( $J_{m}$ is a positive integer), determine $\beta^{*}\left(J_{m}{ }^{*}\right)$ and $\beta^{*}\left(J_{m}{ }^{*}+1\right)$ from Eq. (6.23). Compute $T C^{*}\left(1, J_{m}{ }^{*}, J_{\eta}{ }^{*}\right)$, $T C *\left(1, J_{m}{ }^{*}+1, J_{\eta}{ }^{*}\right), T C^{*}\left(1, J_{m}{ }^{*}, J_{\eta}{ }^{*}+1\right)$ and $T C^{*}\left(1, J_{m}{ }^{*}+1, J_{\eta}{ }^{*}+1\right)$ from Eq. (6.28) and choose the one with smaller value as the optimal solution.
(b) If $n^{*}>1$, then choose $J_{n}{ }^{*}<n^{*}<J_{n}{ }^{*}+1$ (where $J_{n}$ is a positive integer).
7. If $m^{*}<1$, then choose $m^{*}=1$. Determine $\beta^{*}$ (1) from Eq. (6.23). Compute $T C^{*}\left(J_{n}{ }^{*}, 1, J_{\eta}{ }^{*}\right), T C^{*}\left(J_{n}{ }^{*}+1,1, J_{\eta}{ }^{*}\right), T C^{*}\left(J_{n}{ }^{*}, 1, J_{\eta}^{*}+1\right)$ and $T C *\left(J_{n} *+1,1, J_{\eta}{ }^{*}+1\right)$ from Eq. (6.28) and choose the one with smaller value as the optimal solution.
8. If $\mathrm{m}^{*}>1$, and $J_{m}{ }^{*}<m^{*}<J_{m}{ }^{*}+1$ (where $J_{m}$ is a positive integer), determine $\beta^{*}\left(J_{m}{ }^{*}\right)$ and $\beta^{*}\left(J_{m}{ }^{*}+1\right)$ from Eq. (6.23). Compute $T C^{*}\left(J_{n}{ }^{*}\right.$, $\left.J_{m}{ }^{*}, J_{\eta}^{*}\right), T C *\left(J_{n} *+1, J_{m}{ }^{*}, J_{\eta}^{*}\right), T C^{*}\left(J_{n} *, J_{m}{ }^{*}+1, J_{\eta}{ }^{*}\right), T C^{*}\left(J_{n} *+1\right.$, $\left.J_{m}{ }^{*}+1, J_{\eta}{ }^{*}\right), T C^{*}\left(J_{n}{ }^{*}, J_{m}{ }^{*}, J_{\eta}{ }^{*}+1\right), T C^{*}\left(J_{n}{ }^{*}+1, J_{m}{ }^{*}, J_{\eta}^{*}+1\right), T C^{*}\left(J_{n} *\right.$, $\left.J_{m}{ }^{*}+1, J_{\eta}{ }^{*}+1\right)$ and $T C^{*}\left(J_{n} *+1, J_{m}{ }^{*}+1, J_{\eta}{ }^{*}+1\right)$ from Eq. (6.28) and choose the one with smaller value as the optimal solution.

### 6.1.1.3 Single purchase single delivery (SPSD, $m=1$ ) with inspection errors

The SPMD model reduces to SPSD when we substitute $m$ by 1 in SPMD model as shown in Fig. 6.3. The behavior of the raw material and rework inventory in this model remains the same as the SPMD model, but the whole batch of finished goods manufactured in a production run is delivered immediately after production.


Fig. 6.3 Single purchase single delivery (SPSD)

Considering $m=1$ and $x=Q_{f}$ in Eq. (6.18) yields,

$$
\begin{align*}
& T C\left(Q_{f}, n\right)=\frac{i C Q_{f}}{2 f_{0}}\left[\frac{D_{f}}{P}+n-1\right]+\frac{D_{f}}{Q_{f}}\left(\frac{A_{r}}{n}+A_{f}\right)+i(C+V) \frac{Q_{f} D_{f}}{2 P}[1+\beta(1-\beta)]+ \\
& V D_{f}(1+\beta)+D_{f}\left(\pi_{1} E_{1}+\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha Q_{f}}{2 P \theta}\right)+  \tag{6.31}\\
& \frac{i \beta Q_{f} D_{f}}{2 P}(C+V+\beta C+2 \beta V)+Q_{f}\left(C_{i}+\frac{\beta C_{l}}{P}+V \beta\right)
\end{align*}
$$

Differentiating Eq. (6.31) with respect to $n$ and equating the resulting the expression to zero, the optimal value of $n$ is obtained as;
$n^{*}=\frac{1}{Q_{f}} \sqrt{\frac{2 f_{0} D_{f} A_{r}}{i C}}$
Differentiating the Eq. (6.31) with respect to $Q_{f}$ and equating the resulting expression to zero yields;

$$
\begin{aligned}
& \frac{\partial T C\left(Q_{f}, n\right)}{\partial Q_{f}}=\frac{i C}{2 f_{0}}\left[\frac{D_{f}}{P}+n-1\right]-\frac{D_{f}}{Q_{f}^{2}}\left(\frac{A_{r}}{n}+A_{f}\right)+i(C+V) \frac{D_{f}}{2 P}\left[[1+\beta(1-\beta)]+Q_{f} \frac{d \beta}{d Q_{f}}(1-2 \beta)\right]+ \\
& V D_{f} \frac{d \beta}{d Q_{f}}+D_{f}\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha}{2 P \theta}+\frac{i D_{f} \beta}{2 P}(C+V+\beta C+2 \beta V)+ \\
& \frac{i Q_{f} D_{f}}{2 P} \frac{d \beta}{d Q_{f}}(C+V+2 \beta C+4 \beta V)+\left(C_{i}+\frac{\beta C_{l}}{P}+V \beta\right)+Q_{f} \frac{d \beta}{d Q_{f}}\left(\frac{C_{l}}{P}+V\right)=0
\end{aligned}
$$

where $\frac{d \beta}{d Q_{f}}=\frac{\alpha}{2 P \theta}\left(1-E_{1}-E_{2}\right)$

### 6.1.1.4 Single purchase single delivery (SPSD, $m=1$ ) with process inspection and restoration

Considering $m=1$ and $x=Q_{f}$ in Eq. (6.28) for the total cost including inspection and restoration yields,

$$
\begin{align*}
& T C\left(Q_{f}, n, \eta\right)=\frac{i C Q_{f}}{2 f_{0}}\left[\frac{D_{f}}{P}+n-1\right]+\frac{D_{f}}{Q_{f}}\left(\frac{A_{r}}{n}+A_{f}\right)+i(C+V) \frac{Q_{f} D_{f}}{2 P}\left[1+\beta_{i}\left(1-\beta_{i}\right)\right]+ \\
& V D_{f}\left(1+\beta_{i}\right)+D_{f}\left(\pi_{1} E_{1}+\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha Q_{f}}{2 \eta P \theta}\right)+\frac{i \beta_{i} Q_{f} D_{f}}{2 P}\left(C+V+\beta_{i} C+2 \beta_{i} V\right)+ \\
& Q_{f}\left(C_{i}+\frac{\beta_{i} C_{l}}{P}+V \beta_{i}\right)+\frac{D_{f}}{Q_{f}} \eta \nu+\frac{Q_{f} D_{f}}{2 \eta P^{2} \theta^{2}}\left(r_{1} \theta-r_{0}\right)+\frac{D_{f} r_{0}}{P \theta} \tag{6.34}
\end{align*}
$$

Differentiating Eq. (6.31) with respect to $n$ and equating the resulting the expression to zero, the optimal value of $n$ is shown in Eq. (6.32).
Differentiating the Eq. (6.28) with respect to $Q_{f}$ and equating the resulting expression to zero yields;

$$
\begin{align*}
& \frac{\partial T C\left(Q_{f}, n, \eta\right)}{\partial Q_{f}}=\frac{i C}{2 f_{0}}\left[\frac{D_{f}}{P}+n-1\right]-\frac{D_{f}}{Q_{f}^{2}}\left(\frac{A_{r}}{n}+A_{f}\right)+i(C+V) \frac{D_{f}}{2 P}\left[1+\beta_{i}\left(1-\beta_{i}\right)\right]+ \\
& i(C+V) \frac{Q_{f} D_{f}}{2 P}\left(\frac{\partial \beta_{i}}{\partial Q_{f}}-2 \beta_{i} \frac{\partial \beta_{i}}{\partial Q_{f}}\right)+V D_{f} \frac{\partial \beta_{i}}{\partial Q_{f}}+D_{f}\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha}{2 \eta P \theta}+ \\
& \frac{i D_{f}}{2 P}\left(\beta_{i} C+\beta_{i} V+\beta_{i}^{2} C+2 \beta_{i}^{2} V\right)+\frac{i Q_{f} D_{f}}{2 P}\left(\frac{\partial \beta_{i}}{\partial Q_{f}} C+\frac{\partial \beta_{i}}{\partial Q_{f}} V+2 \beta_{i} \frac{\partial \beta_{i}}{\partial Q_{f}} C+4 \beta_{i} \frac{\partial \beta_{i}}{\partial Q_{f}} V\right)+ \\
& \left(C_{i}+\frac{\beta_{i} C_{l}}{P}+V \beta_{i}\right)+Q_{f}\left(\frac{C_{l}}{P} \frac{\partial \beta_{i}}{\partial Q_{f}}+V \frac{\partial \beta_{i}}{\partial Q_{f}}\right)-\frac{D_{f}}{Q_{f}^{2}} \eta \nu+\frac{D_{f}}{2 \eta P^{2} \theta^{2}}\left(r_{1} \theta-r_{0}\right)=0 \tag{6.35}
\end{align*}
$$

where $\frac{\partial \beta_{i}}{\partial Q_{f}}=\frac{\alpha}{2 \eta P \theta}\left(1-E_{1}-E_{2}\right)$
Differentiating the Eq. (6.28) with respect to $\eta$ and equating the resulting expression to zero yields;

$$
\begin{align*}
& \frac{\partial T C\left(Q_{f}, n, \eta\right)}{\partial \eta}=i(C+V) \frac{Q_{f} D_{f}}{2 P}\left(\frac{\partial \beta_{i}}{\partial \eta}-2 \beta_{i} \frac{\partial \beta_{i}}{\partial \eta}\right)+V D_{f} \frac{\partial \beta_{i}}{\partial \eta}-D_{f}\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha Q_{f}}{2 \eta^{2} P \theta}+ \\
& \frac{i Q_{f} D_{f}}{2 P}\left[\frac{\partial \beta_{i}}{\partial \eta}(C+V)+2 \beta_{i} \frac{\partial \beta_{i}}{\partial \eta}(C+2 V)\right]+Q_{f} \frac{\partial \beta_{i}}{\partial \eta}\left(\frac{C_{l}}{P}+V\right)+\frac{D_{f}}{Q_{f}} v-\frac{Q_{f} D_{f}}{2 \eta^{2} P^{2} \theta^{2}}\left(r_{1} \theta-r_{0}\right)=0 \tag{6.36}
\end{align*}
$$

where $\frac{\partial \beta_{i}}{\partial \eta}=-\frac{\alpha Q_{f}}{2 \eta^{2} P \theta}\left(1-E_{1}-E_{2}\right)$

### 6.1.1.5 Lot-for-lot (LFL, $m=1, n=1$ ) with inspection errors

The SPMD model reduces to LFL when both $m$ and $n$ are substituted by 1 in the SPMD model as shown in Fig. 6.4. In this policy, raw material ordering quantity is that required for one lot instead of multiple batches as in SPMD, and the whole production batch is delivered immediately after production. The rework inventory is similar to SPMD. Therefore we have $\mathrm{m}=1$ $\left(\mathrm{x}=\mathrm{Q}_{\mathrm{f}}\right)$ and $\mathrm{n}=1$.

Substituting $\mathrm{x}=\mathrm{Q}_{\mathrm{f}}, \mathrm{m}=1, \mathrm{n}=1$ in Eq. (6.18), we have

$$
\begin{align*}
& T C\left(Q_{f}\right)=\frac{i C Q_{f} D_{f}}{2 f_{0} P}+\frac{D_{f}}{Q_{f}}\left(A_{r}+A_{f}\right)+i(C+V) \frac{Q_{f} D_{f}}{2 P}[1+\beta(1-\beta)]+V D_{f}(1+\beta)+ \\
& D_{f}\left(\pi_{1} E_{1}+\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha Q_{f}}{2 P \theta}\right)+\frac{i \beta Q_{f} D_{f}}{2 P}(C+V+\beta C+2 \beta V)+Q_{f}\left(C_{i}+\frac{\beta C_{l}}{P}+V \beta\right) \tag{6.37}
\end{align*}
$$



Fig. 6.4 Lot-for-Lot (LFL)

Differentiating the Eq. (6.37) with respect to $Q_{f}$ and equating the resulting expression to zero yields;

$$
\begin{align*}
& \frac{\partial T C\left(Q_{f}\right)}{\partial Q_{f}}=\frac{i C D_{f}}{2 f_{0} P}-\frac{D_{f}}{Q_{f}^{2}}\left(A_{r}+A_{f}\right)+i(C+V) \frac{D_{f}}{2 P}\left[[1+\beta(1-\beta)]+Q_{f} \frac{d \beta}{d Q_{f}}(1-2 \beta)\right]+ \\
& V D_{f} \frac{d \beta}{d Q_{f}}+D_{f}\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha}{2 P \theta}+\frac{i D_{f} \beta}{2 P}(C+V+\beta C+2 \beta V)+ \\
& \frac{i Q_{f} D_{f}}{2 P} \frac{d \beta}{d Q_{f}}(C+V+2 \beta C+4 \beta V)+\left(C_{i}+\frac{\beta C_{l}}{P}+V \beta\right)+Q_{f} \frac{d \beta}{d Q_{f}}\left(\frac{C_{l}}{P}+V\right)=0 \tag{6.38}
\end{align*}
$$

### 6.1.1.6 Lot-for-lot (LFL, $m=1, n=1$ ) with process inspection and restoration

Considering $m=1, \mathrm{n}=1$ and $x=Q_{f}$ in Eq. (6.28) for the total cost including inspection and restoration yields,

$$
\begin{align*}
& T C\left(Q_{f}, \eta\right)=\frac{i C Q_{f} D_{f}}{2 f_{0} P}+\frac{D_{f}}{Q_{f}}\left(A_{r}+A_{f}\right)+i(C+V) \frac{Q_{f} D_{f}}{2 P}\left[1+\beta_{i}\left(1-\beta_{i}\right)\right]+ \\
& V D_{f}\left(1+\beta_{i}\right)+D_{f}\left(\pi_{1} E_{1}+\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha Q_{f}}{2 \eta P \theta}\right)+\frac{i \beta_{i} Q_{f} D_{f}}{2 P}\left(C+V+\beta_{i} C+2 \beta_{i} V\right)+ \\
& Q_{f}\left(C_{i}+\frac{\beta_{i} C_{l}}{P}+V \beta_{i}\right)+\frac{D_{f}}{Q_{f}} \eta v+\frac{Q_{f} D_{f}}{2 \eta P^{2} \theta^{2}}\left(r_{1} \theta-r_{0}\right)+\frac{D_{f} r_{0}}{P \theta} \tag{6.39}
\end{align*}
$$

Differentiating the Eq. (6.39) with respect to $Q_{f}$ and equating the resulting expression to zero yields;

$$
\begin{align*}
& \frac{\partial T C\left(Q_{f}, \eta\right)}{\partial Q_{f}}=\frac{i C D_{f}}{2 f_{0} P}-\frac{D_{f}}{Q_{f}^{2}}\left(A_{r}+A_{f}\right)+i(C+V) \frac{D_{f}}{2 P}\left[1+\beta_{i}\left(1-\beta_{i}\right)\right]+ \\
& i(C+V) \frac{Q_{f} D_{f}}{2 P}\left(\frac{\partial \beta_{i}}{\partial Q_{f}}-2 \beta_{i} \frac{\partial \beta_{i}}{\partial Q_{f}}\right)+V D_{f} \frac{\partial \beta_{i}}{\partial Q_{f}}+D_{f}\left(s-s E_{2}-\pi_{1} E_{1}+\pi_{2} E_{2}\right) \frac{\alpha}{2 \eta P \theta}+ \\
& \frac{i D_{f}}{2 P}\left(\beta_{i} C+\beta_{i} V+\beta_{i}{ }^{2} C+2 \beta_{i}{ }^{2} V\right)+\frac{i Q_{f} D_{f}}{2 P}\left(\frac{\partial \beta_{i}}{\partial Q_{f}} C+\frac{\partial \beta_{i}}{\partial Q_{f}} V+2 \beta_{i} \frac{\partial \beta_{i}}{\partial Q_{f}} C+4 \beta_{i} \frac{\partial \beta_{i}}{\partial Q_{f}} V\right)+ \\
& \left(C_{i}+\frac{\beta_{i} C_{l}}{P}+V \beta_{i}\right)+Q_{f}\left(\frac{C_{l}}{P} \frac{\partial \beta_{i}}{\partial Q_{f}}+V \frac{\partial \beta_{i}}{\partial Q_{f}}\right)-\frac{D_{f}}{Q_{f}^{2}} \eta v+\frac{D_{f}}{2 \eta P^{2} \theta^{2}}\left(r_{1} \theta-r_{0}\right)=0 \tag{6.40}
\end{align*}
$$

Differentiating the Eq. (6.39) with respect to $\eta$ and equating the resulting expression to zero results in Eq. (6.36).

### 6.1.2 Numerical computation

Consider a manufacturing system with the following data (Ojha et al., 2007 and Ben-Daya and Rahim, 2003): $\mathrm{E}_{1}=0.1$, and $\mathrm{E}_{2}=0.1, \mathrm{~A}_{\mathrm{f}}=\$ 50$ per setup, $\mathrm{A}_{\mathrm{r}}=\$ 150$ per order, $\mathrm{C}=\$ 2$ per unit, $\mathrm{C}_{\mathrm{i}}=\$ 0.2$ per unit, $C_{1}=\$ 0.1$ per unit time, $D=2000$ units per year, $f_{0}=0.95, \mathrm{i}=0.18, \mathrm{P}=3000$ units per year, $\mathrm{V}=\$ 1$ per unit, $v=0.05 \mathrm{~A}_{\mathrm{f}}, \alpha=0.05, \theta=0.05, \mathrm{~s}=\mathrm{V}, \pi_{1}=0.5 \mathrm{~V}, \pi_{2}=1.5 \mathrm{~V}, \mathrm{r}_{0}=0.15 \mathrm{~A}_{\mathrm{f}}, \mathrm{r}_{1}=0.01 \mathrm{~A}_{\mathrm{f}}$.

Table 6.1 shows the optimal batch size and expected total cost for (i) imperfect production process with quality and rework, and the optimal number inspections, batch size and total cost for (ii) imperfect production process with quality and rework including process inspection and restoration for the following: (a) SPMD policy when the delivery size of finished product is $\mathrm{x}=20$ units, (b) the SPSD policy, and (c) the LFL policy. The optimal batch size, ordering quantity and total cost increases for SPMD, SPSD and LFL policies by incorporating inspection and restoration of the process in the imperfect production process with quality and rework. The optimal number of inspections increases with increase in the optimal batch size and ordering quantity. The optimal expected total cost also reduces for SPMD and LFL policies for the given data by including process inspection and restoration.

Table 6.1 Optimal batch size and expected total cost

|  | Imperfect production process <br> with quality and rework |  |  | Imperfect production process with <br> quality and rework including <br> process inspection and restoration |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | SPMD | SPSD | LFL | SPMD | SPSD | LFL |
|  | 5 | 4 | - | 4 | 4 | - |
| N | 13 | - | - | 15 | - | - |
| M | - | - | - | 3 | 3 | 5 |
| H | 260 | 293 | 528 | 300 | 335 | 571 |
| $\mathrm{Q}_{\mathrm{f}}$ | 274 | 309 | 555 | 316 | 352 | 601 |
| $\mathrm{Q}_{\mathrm{r}}$ |  |  |  |  |  |  |
| Expected Total <br> Cost (ETC) | 3512.78 | 3443.67 | 3765.00 | 3496.45 | 3496.30 | 3707.50 |

The optimal number of inspections, batch quantity and cost and are studied by varying the parameters such as the (i) fraction of nonconforming units ( $\alpha$ ), (ii) value added by the manufacturing process (V), (iii) type I inspection error ( $\mathrm{E}_{1}$ ), and (iv) type II inspection error ( $\mathrm{E}_{2}$ ). Table 6.2 and 6.3 show the influence of fraction of non-conforming units $(\alpha)$ on the optimal ordering quantity and optimal cost. It can be seen that as the fraction of non-conforming units increases, the optimal ordering quantity decreases, while the optimal expected total cost increases for SPMD, SPSD, and LFL policies. Incorporating process inspection and restoration increases optimal ordering quantity and reduces the optimal expected total cost for SPMD, SPSD, and LFL policies. This is owing to reduction in the expected number of non-conforming items produced incorporating process inspection and restoration. With increase in the fraction of non-conforming units ( $\alpha$ ) optimal number of inspections increase, while the optimal ordering quantity decreases and optimal expected total cost increases for SPMD, SPSD, and LFL policies. For the data considered the optimal number of inspections are lower for SPMD and SPSD policies, while optimal number of inspections are higher for LFL policy. For all the values of fraction of non-conforming units, the optimal ordering quantity is smaller for SPMD and SPSD, and larger for LFL.

Table 6.2 Effect of fraction of non-conforming units ( $\alpha$ ) with quality and rework

|  | Imperfect production process with quality and rework |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | SPMD | SPSD | LFL |  |  |  |
| $\alpha$ | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\mathrm{Q}_{\mathrm{r}}$ | ETC |
| 0.05 | 274 | 3512.78 | 309 | 3443.67 | 555 | 3765.00 |
| 0.10 | 232 | 3667.44 | 247 | 3612.43 | 453 | 4090.68 |
| 0.25 | 168 | 4015.78 | 172 | 3977.98 | 324 | 4808.27 |
| 0.40 | 147 | 4287.87 | 140 | 4254.05 | 267 | 5352.84 |
| 0.50 | 126 | 4438.64 | 127 | 4411.56 | 243 | 5665.05 |

Table 6.3 Effect of fraction of non-conforming units ( $\alpha$ ) with quality and rework including inspection and restoration

|  | Imperfect production process with quality and rework including process inspection and restoration |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SPMD |  |  | SPSD |  |  | LFL |  |  |
| $\alpha$ | $\eta$ | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\eta$ | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\eta$ | $\mathrm{Q}_{\mathrm{r}}$ | ETC |
| 0.05 | 3 | 316 | 3496.45 | 3 | 352 | 3496.30 | 5 | 601 | 3707.50 |
| 0.10 | 4 | 274 | 3581.50 | 4 | 279 | 3584.05 | 7 | 491 | 3826.40 |
| 0.25 | 5 | 189 | 3796.07 | 5 | 194 | 3791.10 | 9 | 352 | 4145.76 |
| 0.40 | 5 | 168 | 3918.75 | 5 | 158 | 3958.05 | 9 | 290 | 4417.38 |
| 0.50 | 5 | 147 | 4031.10 | 5 | 143 | 4055.59 | 9 | 263 | 4579.70 |

Table 6.4 and 6.5 show the impact of value added by the manufacturing process $(\mathrm{V})$ on the SPMD, SPSD and LFL policies. The more the value added by the manufacturing process V , the higher will be the expected optimal expected total cost. With increase in the value added by the manufacturing process, the optimal batch size decreases while the expected total cost increases for the SPMD, SPSD and LFL policies. The optimal number of inspections increases with the increase in the value added by the manufacturing process for all the SPMD, SPSD and LFL policies. The optimal number of inspections are higher LFL policy while lower for SPMD and SPSD policies.

Table 6.4 Effect of value added by the manufacturing process (V) with quality and rework

|  | Imperfect production process with quality and rework |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SPMD |  | SPSD |  | LFL |  |
| V | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\mathrm{Q}_{\mathrm{r}}$ | ETC |
| 1.0 | 274 | 3512.78 | 309 | 3443.67 | 555 | 3765.00 |
| 4.0 | 168 | 10933.19 | 176 | 10857.67 | 334 | 11654.60 |
| 6.0 | 147 | 15784.22 | 146 | 15697.78 | 281 | 16728.37 |
| 8.0 | 126 | 20593.97 | 128 | 20503.56 | 248 | 21733.70 |

Table 6.5 Effect of value added by the manufacturing process ( $V$ ) with quality and rework including inspection and restoration

|  | Imperfect production process with quality and rework including process inspection and restoration |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SPMD |  |  | SPSD |  |  | LFL |  |  |
| V | $\eta$ | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\eta$ | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\eta$ | $\mathrm{Q}_{\mathrm{r}}$ | ETC |
| 1.0 | 3 | 316 | 3496.45 | 3 | 352 | 3496.30 | 5 | 601 | 3707.50 |
| 4.0 | 4 | 189 | 10801.96 | 4 | 196 | 10803.96 | 8 | 359 | 11266.94 |
| 6.0 | 4 | 168 | 15575.60 | 4 | 163 | 15599.50 | 8 | 301 | 16201.63 |
| 8.0 | 4 | 147 | 20337.76 | 4 | 142 | 20367.77 | 8 | 264 | 21092.79 |

Table 6.6 and 6.7 show the influence of type I inspection errors. As the inspection errors increase, the optimal ordering quantity decreases while the optimal expected total cost increases. Incorporating process inspection and rework increases the optimal ordering quantity for all the SPMD, SPSD and LFL policies. The optimal number of inspections decreases with increase in the type I inspection errors due the reduction in the ordering quantity.

Table 6.6 Effect of type I inspection error $\left(\mathbf{E}_{1}\right)$ with quality and rework

|  | Imperfect production process with quality and rework |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | SPMD | SPSD | LFL |  |  |  |
|  | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\mathrm{Q}_{\mathrm{r}}$ | ETC |
|  | 274 | 3512.78 | 309 | 3443.67 | 555 | 3765.00 |
|  | 274 | 3834.16 | 300 | 3768.47 | 544 | 4104.95 |
|  | 253 | 4797.74 | 275 | 4735.28 | 512 | 5123.68 |

Table 6.7 Effect of type I inspection error $\left(E_{1}\right)$ with quality and rework including inspection and restoration

|  | Imperfect production process with quality and rework including process inspection and restoration |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SPMD |  |  | SPSD |  |  | LFL |  |  |
| $\mathrm{E}_{1}$ | $\eta$ | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\eta$ | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\eta$ | $\mathrm{Q}_{\mathrm{r}}$ | ETC |
| 0.10 | 3 | 316 | 3496.45 | 3 | 352 | 3496.30 | 5 | 601 | 3707.50 |
| 0.20 | 3 | 316 | 3827.85 | 3 | 340 | 3830.83 | 5 | 585 | 4077.41 |
| 0.50 | 2 | 274 | 4806.39 | 2 | 313 | 4816.46 | 3 | 545 | 5172.13 |

Table 6.8 and 6.9 show the influence of type II inspection errors. As the type II inspection errors increase, the optimal ordering quantity increases while the optimal expected total cost reduces.

Incorporating process inspection and rework increases the optimal ordering quantity for all the SPMD, SPSD and LFL policies.

Table 6.8 Effect of type II inspection error $\left(E_{2}\right)$ with quality and rework

|  | Imperfect production process with quality and rework |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | SPMD | SPSD | LFL |  |  |  |
|  | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\mathrm{Q}_{\mathrm{r}}$ | ETC |
|  | 274 | 3512.78 | 309 | 3443.67 | 555 | 3765.00 |
|  | 274 | 3506.90 | 313 | 3436.37 | 563 | 3749.65 |
|  | 274 | 3476.45 | 326 | 3414.17 | 589 | 3701.72 |

Table 6.9 Effect of type II inspection error $\left(\mathbf{E}_{2}\right)$ with quality and rework including inspection and restoration

|  | Imperfect production process with quality and rework including process inspection and restoration |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SPMD |  |  | SPSD |  |  | LFL |  |  |
| $\mathrm{E}_{2}$ | $\eta$ | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\eta$ | $\mathrm{Q}_{\mathrm{r}}$ | ETC | $\eta$ | $\mathrm{Q}_{\mathrm{r}}$ | ETC |
| 0.10 | 3 | 316 | 3496.45 | 3 | 352 | 3496.30 | 5 | 601 | 3707.50 |
| 0.20 | 3 | 337 | 3487.13 | 3 | 357 | 3492.18 | 5 | 608 | 3701.02 |
| 0.50 | 3 | 337 | 3473.36 | 3 | 373 | 3479.24 | 5 | 633 | 3680.11 |



Fig. 6.5 Variation of ETC with $\alpha$ and V


Fig. 6.6 Variation of ETC with $E_{1}$ and $E_{2}$

Figures 6.5 and 6.6 show the variation of expected total cost (ETC) for single purchase multiple delivery (SPMD) policy under quality and rework including inspection and restoration. Figure 6.5 shows the increase in expected total cost (ETC) with both fraction of nonconforming units $(\alpha)$ and value added by the manufacturing process $(\mathrm{V})$ respectively. The increase in ETC with V is much higher compared to the increase in ETC with $\alpha$. Figure 6.6 variation of (ETC) with both $E_{1}$ and $E_{2}$ respectively. For given value of $E_{2}$, ETC increases with increase in $E_{1}$, while for a given value of $\mathrm{E}_{1}$, ETC decreases with increase in $\mathrm{E}_{2}$.

### 6.2 Optimal Batch Size in a Single-Stage Imperfect Production-Delivery System with

## Rework

Sarker and Parija (1996) developed an ordering policy for raw materials, to meet the demands of a production facility which supplies a fixed quantity of finished products to outside buyers, at a fixed interval of time. They derived the cost function which consists of raw material and finished goods inventory. Their model assumes that a production facility purchases raw materials from outside suppliers and processes them to deliver a fixed quantity of finished products to a buyer at a fixed interval of time. A multi-order policy for procuring raw materials may lower inventory carrying cost because this policy results in a lower inventory carrying cost. Ideally, a manufacturer is expected both to synchronize production with the buyer's lumpy demand and to coordinate the ordering of raw materials with production schedules so that both raw materials and finished goods inventory are reduced. Sarker et al., (2008) developed models for the optimum batch quantity in a multi-stage system with rework process for two different operational policies: (i) the rework within the same cycle with no shortage and (ii) the rework done after N cycles, incurring shortages in each cycle. In the policy (i), an economic batch quantity model for defective items that are reworked within the same cycle is developed to avoid penalty cost incurred due to shortage. In the policy (ii), the defective items from each cycle are accumulated for a certain number of cycles before they are reworked. Some amount of shortage occurs in each cycle due to the production of defectives and hence a penalty cost is imposed for not correctly meeting the demand of good finished products after each cycle.

In this research, Sarker and Parija's (1996) model is extended by considering the reworking of defects in the same cycle and the total cost function is derived. The total cost function is
minimized to determine the optimal batch size and production run length for a single-stage production system.

The remainder of the section is organized as follows. The assumptions and necessary notation are described. Mathematical model and numerical results for single-stage production-delivery system with rework are provided.

The notations used are defined as follows:
$C_{f} \quad$ rework processing cost, $\$$
$D_{f} \quad$ demand of finished goods, units/year
$D_{r} \quad$ demand of the raw materials, units/year
$f \quad$ indicates a ratio of the quantity (or demand) of finished goods to the quantity (or demand) of raw materials required to produce that quantity of finished goods $\left(f=D_{F} / D_{r}=Q_{f} \not Q_{r}\right)$
$H_{f} \quad$ finished goods holding cost, \$/unit-year
$H_{o} \quad$ raw materials holding carrying cost, \$/unit-year
$I(t) \quad$ inventory level, units
$K_{o} \quad$ ordering cost of the raw materials, $\$ /$ order
$K_{s} \quad$ manufacturing setup cost for each batch, \$/batch
$L_{f} \quad$ time between successive shipments of finished goods
$m_{f} \quad$ number of full shipments of finished goods per cycle
$n_{o} \quad$ number of orders for raw materials during uptime $T_{1}\left(n_{o}=D_{r} / Q_{o}\right)$
$P_{f} \quad$ production rate, units/year
$Q_{\text {avg }} \quad$ average inventory of finished goods per cycle, units
$Q_{f} \quad$ quantity of finished goods manufactured per setup, units/batch
$Q_{o} \quad$ quantity of raw materials ordered each time, $\left(Q_{o}=Q_{v} / n\right)$
$Q_{r} \quad$ quantity of raw materials required for each batch, $\left(Q_{r}=Q_{f} / f=n Q_{o}\right)$
$Q_{s} \quad$ quantity of finished goods shipped
$T \quad$ cycle time, $\left(T=Q_{f} / D_{f}=m_{f} L\right)$
$T_{1} \quad$ quantity of goods manufactured during the production uptime ( $\left.T_{l}=Q_{f} / P_{f}=m_{f} L\right)$
$x_{f} \quad$ fixed quantity of finished goods per shipment at a fixed interval of time, units/ shipment, $\left(x_{f}=Q_{f} / m=L D_{f}\right)$
$\beta_{f} \quad$ proportion of defectives produced in the stage

The assumptions in the model are

1. The model assumes that a production facility purchases raw materials from outside suppliers and processes them to deliver a fixed quantity of finished products to a buyer at a fixed interval of time.
2. The annual demand of this buyer is known and fixed.
3. The production rate of the facility is assumed to be greater than the demand rate so as to ensure no shortage of products due to insufficient production.
4. The raw material is nonperishable, and it is supplied instantaneously to the manufacturing facility.
5. Proportion of defective is constant in each cycle.
6. No product is scraped at any cycle.
7. No defectives are produced during the rework.
8. Inspection cost is ignored.
9. Cost of processing of jobs on the machine is ignored.

### 6.2.1 Model formulation for single-stage production-delivery system with rework

This model incorporates the rework in the production-delivery model considered by Sarker and Parija (2006). The behavior of raw material ordering and finished goods demand in this problem is different from the behavior in a traditional economic batch quantity model with continuous demand. A multi-order policy for procuring raw materials and fixed quantity of finished goods demand at regular intervals are considered. The total inventory costs of raw materials and finished goods in the production-delivery system are minimized to determine an (1) optimal raw materials order quantity, $\mathrm{Q}_{\mathrm{o}}$, procured during the uptime, $\mathrm{T}_{1}$, (2) optimal finished goods quantity, $\mathrm{Q}_{\mathrm{f}}$, so that production with single setup meets the demand for that cycle, and (3) the rework of a defective item is done in the same cycle.

Raw materials are procured and converted to finished goods during the productive time, $\mathrm{T}_{1}$. The manufacturer has a yearly demand of $D_{r}$ units of raw materials in order to meet a yearly demand of $D_{f}$ units of finished goods by buyers. The amount of raw materials ordered during any cycle
should meet the requirements for production within that cycle. Raw materials must not be carried during the downtime period, $\left(\mathrm{T}_{1}, \mathrm{~T}\right)$, while finished goods may build up during the uptime period and deplete during the downtime period until reaching zero at the end of the cycle time, T.
Fig. 6.7 shows the raw material ordering quantity during uptime, $T_{1}$. The cost of raw material inventory is given by (Sarker and Parija, 1996)

$$
\begin{align*}
& T C_{r}=\frac{D_{r} K_{0}}{Q_{o}}+\frac{Q_{o} T_{1} H_{0}}{2 T}=\frac{D_{r} n_{0} K_{0}}{Q_{r}}+\frac{Q_{r} D_{f} H_{0}}{2 n_{0} P_{f}}=\frac{D_{f} n_{0} K_{0}}{Q_{f}}+\left(\frac{Q_{r}}{Q_{f}}\right) \frac{Q_{f} D_{f} H_{0}}{2 n_{0} P_{f}}=  \tag{6.41}\\
& \frac{D_{f} n_{0} K_{0}}{m_{f} x_{f}}+\frac{m_{f} x_{f} D_{f} H_{0}}{2 f n_{0} P_{f}}
\end{align*}
$$



Fig. 6.7 Raw material inventory level in a single-stage production system

Fig. 6.8 shows the finished goods inventory. The derivation of average finished goods inventory is given in Appendix D.1.
$T C_{f}=\frac{D_{f} K_{s}}{Q_{f}}+Q_{\text {avg }} H_{f}=\frac{D_{f} K_{s}}{m_{f} x_{f}}+\frac{1}{2}\left\{m_{f} x_{f}\left(1-\frac{D_{f}}{P_{f}}\right)+x_{f}\right\} H_{f}$


Fig. 6.8 Finished goods inventory level in a single-stage production system

The total cost is obtained as (Sarker and Parija, 1996 )
$T C\left(m_{f}, n_{0}\right)=\frac{D_{f}\left(n_{0} K_{0}+K_{s}\right)}{m_{f} x_{f}}+\frac{m_{f} x_{f} D_{f} H_{0}}{2 f n_{0} P_{f}}+\frac{1}{2}\left\{m_{f} x_{f}\left(1-\frac{D_{f}}{P_{f}}\right)+x_{f}\right\} H_{f}$
Defective items be produced in the stage are reworked within the same cycle at the same stage. Costs are involved in rework of defective products. When defective items are processed in a stage, the inventory of reworked items builds up, incurring carrying costs as well. The rework processing cost per cycle for $\beta_{f} Q_{f}$ units of defective items reworked in the stage can be written as $Q_{f} \beta_{f} C_{f}$. Hence reprocessing cost over the planning period is $Q_{f}\left(D_{f} / Q_{f}\right) \beta_{f} C_{f}=D_{f} \beta_{f} C_{f}$ The total cost considering the reworking of defects in the same cycle is obtained as
$T C=\frac{D_{r} K_{o}}{Q_{o}}+I_{\text {avg }} H_{o}+\frac{D_{f} K_{s}}{Q_{f}}+D_{f} \beta_{f} C_{f}+Q_{\text {avg }} H_{f}$

Substituting $\quad I_{\text {avg }}=\frac{Q_{o} T_{1}}{2 T}, \quad \frac{T_{1}}{T}=\frac{D_{f}}{P_{f}}, \quad Q_{o}=\frac{Q_{r}}{n_{o}}, \quad Q_{f}=m_{f} x_{f}, \quad f=\frac{Q_{f}}{Q_{r}}=\frac{m_{f} x_{f}}{Q_{r}}$, $\frac{D_{r}}{Q_{r}}=\frac{D_{f}}{Q_{f}}=\frac{D_{f}}{m_{f} x_{f}}$ and $Q_{\text {avg }}=\frac{1}{2}\left\{m_{f} x_{f}\left(1-\frac{D_{f}\left(1+\beta_{f}-\beta_{f}^{2}\right)}{P_{f}}\right)+x_{f}\right\}$

The derivation of average finished goods inventory with rework is given in Appendix D.2. The expression for the total cost is obtained as

$$
\begin{align*}
& T C\left(m_{f}, n_{0}\right)=\frac{D_{f}\left(n_{0} K_{0}+K_{s}\right)}{m_{f} x_{f}}+\frac{m_{f} x_{f} D_{f} H_{0}}{2 f n_{0} P_{f}}+D_{f} \beta_{f} C_{f} \\
& +\frac{1}{2}\left\{m_{f} x_{f}\left(1-\frac{D_{f}\left(1+\beta_{f}-\beta_{f}^{2}\right)}{P_{f}}\right)+x_{f}\right\} H_{f} \tag{6.45}
\end{align*}
$$

The total cost function is convex as shown in Appendix D.3.
The optimal number orders of raw materials and the optimal number of shipments are

$$
\begin{align*}
& n_{0}^{*}=m_{f} x_{f} \sqrt{\frac{H_{0}}{2 P_{f} f K_{0}}}  \tag{6.46}\\
& m_{f}^{*}=\frac{1}{x_{f}} \sqrt{\frac{2 D_{f} K_{s}}{\left(1-\frac{D_{f}}{P_{f}}\left(1+\beta_{f}-\beta_{f}^{2}\right)\right) H_{f}}} \tag{6.47}
\end{align*}
$$

If $n_{o}>1$ and $m_{f}>1$ then choose $j<n_{o}<j+1$ and $j<m_{f}<j+1$ where $j$ is a positive integer.

### 6.2.2 Computational results

Assume that the proportion of defective items $\beta_{f}$ in the stage is 0.01 and the rework processing cost $C_{f}$ in the stage is $\$ 10.0$. Table 6.10 provides the input data for a single-stage production system (Sarker and Parija, 2006). The comparison of the optimal results and modified results for a single-stage production system with rework consideration are shown in Tables 6.11 and 6.12 respectively. The optimal results for $m_{f}, n_{0}, T_{1}, T, T C$ show a marginal increase with rework consideration in the single-stage production system. The modified results for $m_{f}, n_{0}, T_{1}, T$ with and without rework consideration in the single-stage production system are similar except in few cases where they show marginal increase with rework consideration. For both the optimal and modified results, the total cost for rework in the system is high as the rework processing cost is also considered.

Table 6.10 Input data for a single-stage production system ( $\beta_{f}=0.01, C_{f}=10$ )

| Problem | $D_{f}$ | $P_{f}$ | $K_{0}$ | $K_{s}$ | $H_{0}$ | $H_{f}$ | $x_{f}$ | $F$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 1 | 1200 | 2400 | 50 | 150 | 2 | 3 | 50 | 0.8 |
| 2 | 1500 | 1800 | 100 | 200 | 4 | 8 | 75 | 0.6 |
| 3 | 2400 | 3600 | 100 | 300 | 1 | 2 | 100 | 0.5 |
| 4 | 2400 | 6000 | 100 | 200 | 5 | 10 | 100 | 0.5 |
| 5 | 3600 | 7200 | 300 | 400 | 2 | 2 | 50 | 0.8 |
| 6 | 2000 | 2500 | 100 | 200 | 10 | 15 | 100 | 1.5 |
| 7 | 1000 | 1500 | 400 | 300 | 2 | 10 | 50 | 0.2 |
| 8 | 1200 | 2400 | 50 | 200 | 2 | 3 | 50 | 1.0 |
| 9 | 2500 | 3000 | 100 | 50 | 5 | 15 | 100 | 0.5 |
| 10 | 4000 | 5000 | 50 | 200 | 1 | 10 | 100 | 1.0 |

Table 6.11 Comparison of optimum results for a single-stage production system

| S. No. | Sarker and Parija (1996) |  |  |  | Present <br> consideration) |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | $m_{f}$ | $n_{0}$ | $T_{l}$ | $T$ | $T C$ | $m_{f}$ | $n_{0}$ | $T_{l}$ | $T$ |
| (with | rework |  |  |  |  |  |  |  |  |  |
| 1 | 9.79 | 1.58 | 0.204 | 0.408 | 1197 | 9.85 | 1.58 | 0.205 | 0.410 | 1314 |
| 2 | 8.94 | 2.89 | 0.373 | 0.447 | 2485 | 9.17 | 2.96 | 0.382 | 0.459 | 2613 |
| 3 | 14.70 | 2.45 | 0.408 | 0.612 | 1879 | 14.84 | 2.47 | 0.412 | 0.619 | 2110 |
| 4 | 4.00 | 1.15 | 0.066 | 0.166 | 4285 | 4.01 | 1.16 | 0.067 | 0.167 | 4518 |
| 5 | 33.90 | 1.29 | 0.235 | 0.471 | 3390 | 34.11 | 1.30 | 0.237 | 0.474 | 3742 |
| 6 | 5.16 | 1.88 | 0.206 | 0.258 | 3760 | 5.27 | 1.92 | 0.211 | 0.264 | 3929 |
| 7 | 8.48 | 1.22 | 0.283 | 0.424 | 3973 | 8.57 | 1.28 | 0.286 | 0.429 | 4060 |
| 8 | 11.30 | 1.63 | 0.235 | 0.471 | 1269 | 11.37 | 1.64 | 0.237 | 0.474 | 1388 |
| 9 | 3.16 | 1.29 | 0.105 | 0.126 | 3581 | 3.24 | 1.32 | 0.108 | 0.130 | 3812 |
| 10 | 8.94 | 1.26 | 0.179 | 0.223 | 2854 | 9.13 | 1.29 | 0.183 | 0.228 | 3219 |

Table 6.12 Comparison of modified results for a single-stage production system

| S. <br> No. | Sarker and Parija (1996) |  |  |  | $m_{f}$ | $n_{0}$ | $T_{l}$ | $T$ | $T C$ | $m_{f}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | $T_{l}$ | $T$ | $T C$ |  |  |  |  |  |  |  |
| 1 | 10 | 2 | 0.208 | 0.417 | 1206 | 10 | 2 | 0.208 | 0.417 | 1323 |
| 2 | 9 | 3 | 0.375 | 0.450 | 2486 | 9 | 3 | 0.375 | 0.450 | 2614 |
| 3 | 14 | 2 | 0.388 | 0.583 | 1890 | 14 | 2 | 0.389 | 0.583 | 2121 |
| 4 | 4 | 1 | 0.067 | 0.167 | 4300 | 4 | 1 | 0.067 | 0.167 | 4532 |
| 5 | 33 | 1 | 0.229 | 0.458 | 3433 | 34 | 1 | 0.236 | 0.472 | 3796 |
| 6 | 5 | 2 | 0.200 | 0.250 | 3766 | 5 | 2 | 0.200 | 0.250 | 3937 |
| 7 | 8 | 1 | 0.267 | 0.400 | 4000 | 8 | 1 | 0.267 | 0.400 | 4087 |
| 8 | 12 | 2 | 0.250 | 0.500 | 1275 | 12 | 2 | 0.250 | 0.500 | 1391 |
| 9 | 3 | 1 | 0.100 | 0.120 | 3625 | 3 | 1 | 0.100 | 0.120 | 3856 |
| 10 | 8 | 1 | 0.160 | 0.200 | 2870 | 9 | 1 | 0.180 | 0.225 | 3236 |

### 6.3 Optimal Number of Kanbans in a Multi-Stage JIT Production-Delivery System with

 Rework ConsiderationWang and Sarker (2006) studied a multi-stage supply chain system linked by kanban mechanism that operates under a just-in-time delivery policy. They derived a cost function which consists of the cost of raw materials at the first stage, the cost of WIP in the intermediate stages, and the cost of finished goods at the last stage. The deliveries of raw materials from the suppliers, the work-in-process (WIP) in production stage, and the transshipments of finished goods to retailers are all controlled by the kanbans. The kanban is a practical tool for implementation of JIT delivery in supply chain operations. Kanbans are used as a means for production control and process improvement. In production control, kanbans tie different manufacturing processes and ensure that the delivery of necessary amounts of material and parts at the appropriate time and place. In process improvement, kanbans improves the operations in the production process with emphasis on reducing inventory costs. In a multi-stage production system, products move from one stage to the next stage, and every stage may yield a certain proportion of defective items. The nonreworked items become waste, creating additional costs for producers. Sarker et al., (2008) developed models for an optimal batch quantity for a manufacturing system that allows rework of defective items under two operational policies-reworking defectives within the same cycle and after N cycles. Their results show that the optimal quantity increases with defects in both policies.

In this research, Wang and Sarker's (2006) model is extended by considering the rework processing cost of defects per cycle for all stages and the total cost function is derived with an objective to determine the optimal batch quantity and number of kanbans in a multi-stage production system. The suppliers provide the manufacturers with the raw materials that are processed to manufacture end products that are finally shipped to retailers. The deliveries of raw materials from the suppliers, the work-in-process (WIP) in production stage, and the shipments of finished goods to retailers are all controlled by kanban mechanism.

The remainder of the section is organized as follows. The assumptions and notation are provided. Mathematical model formulation for multi-stage production-delivery system with rework controlled by kanban mechanism is described. Results for a multi-stage production-delivery controlled by kanban mechanism with rework consideration are described.

The notation used in this section are as follows
$D$ demand rate, units/year
$f \quad$ ratio of the quantity of finished goods to the quantity of raw materials
$H_{o} \quad$ holding cost of raw material inventory, \$/unit/year
$H_{i} \quad$ holding cost of work-in-process inventory at stage $i$, \$/unit/year
$i \quad$ an index of a production stage, $i=1,2, \ldots \ldots . . N+1$
$I(t) \quad$ inventory level, units
$K_{o} \quad$ setup (ordering) cost, \$/setup (order)
$K_{i s} \quad$ setup (manufacturing) cost at stage $i, \$ /$ batch
$K_{\text {io }} \quad$ setup (shipping) cost at stage $i, \$ /$ setup (ship)
$m_{i} \quad$ number of shipments (kanbans) at stage $i$
$m_{N+1}$ number of shipments of finished goods at the last production system
$n_{o} \quad$ number of orders of raw material inventory placed
$P_{1} \quad$ production rate of the first production system, units/year
$P_{i} \quad$ production rate of the $\mathrm{i}^{\text {th }}$ production system, units/year
$P_{N+1} \quad$ production rate of the last $\left(\mathrm{N}+1^{\text {th }}\right)$ production system, units/year
$Q_{f} \quad$ quantity of finished goods produced over a period, units/year
$Q_{0} \quad$ quantity of raw material ordered each time, $Q_{0}=Q_{r} / n_{0}$
$Q_{i o} \quad$ quantity of inventory per shipment at a fixed interval of time, $Q_{i o}=Q_{i} / m_{i}$
$T$ cycle time, year
$T_{u i} \quad$ uptime of the $\mathrm{i}^{\text {th }}$ production system, year
$T C_{f} \quad$ cost of finished goods inventory, $\$ /$ year
$T C_{r} \quad$ cost of raw material inventory, \$/year
$T C_{w i} \quad$ cost of work-in-process inventory at $\mathrm{i}^{\text {th }}$ production system, $\$ /$ year
TC total cost of multi-stage production system, \$/year
$\beta_{i} \quad$ proportion of defectives in stage $i$

The assumptions made in the analysis are
(1) The demands of the system are known
(2) The production rate of each stage is known and it is larger than the demand rate
(3) The total quantity of the products at each stage over a period are constant
(4) Shortage is not allowed at any stage
(5) The demand of raw material inventory for the products at the first stage is $p_{1}$, the production rate of stage 1 . The orders arrive in lots on time when the orders are placed. Shortage is not allowed. So the input rate (replenishment) is considered infinite. The company orders raw materials in batches, i.e., EOQ is divided into a number of equal batches, $\mathrm{n}_{\mathrm{o}}$. When the production starts, the shipment (one batch) is set at a fixed interval during one period.
(6) The production at stage $i$ is carried at a rate of $p_{i}$ units/year. The parts produced by this stage are work-in-process inventories built-up before they are shipped. As the stock level reaches the lot size $\mathrm{Q}_{\mathrm{wi}}$, the parts are carried by containers from stage i to $\mathrm{i}+1$. The semifinished parts shipped to stage i from the preceding stage are input to this stage.

The throughput of the plant $\mathrm{N}+1$ is the finished goods of the N -stage production system. The total stock of the finished goods increases at a rate $\mathrm{p}_{\mathrm{N}+1}$.
(8) In a multi-stage system, defective items may be produced in each stage, and they are reworked within the same cycle at the same stage. Proportion of defective for a particular stage remains the same in each cycle for the whole planning period but may be different from that in other stages..
(9) No product is scraped at any cycle.
(10) No defectives are produced during the rework.
(11) Inspection cost is ignored.
(12) Cost of processing of jobs on the machine is ignored.

### 6.3.1 Model formulation for multi-stage production-delivery system with rework controlled by kanban mechanism

Defective units that are to be reworked at every stage are $\beta_{i} Q_{f}$ units. For all n stages the rework processing cost per cycle can be written as $Q_{f} \sum_{i=1}^{N+1} \beta_{i} C_{i}$. Hence rework processing cost over the planning period is $Q_{f} \sum_{i=1}^{N+1}\left(D / Q_{f}\right) \beta_{i} C_{i}=D \sum_{i=1}^{N+1} \beta_{i} C_{i}$

The batch size and the number of batches in each stage is related to the production batch size $Q_{f}$. The total quantity of products produced in each stage over a period T, $Q_{f}$, is assumed to be the same, i.e., $Q_{f}=m_{i} Q_{i o}$.

### 6.3.1.1 Cost of raw material inventory

The raw material inventory arrives in lots on time when the order is placed. The raw materials are ordered in equal number of batches. It is assumed that the demand rate for the raw material inventory for the products at the first production stage is equal to that of the production rate of the first production stage. The raw material inventory model is illustrated in Fig. 6.9 (Wang and Sarker, 2006). The total raw material cost is written as (Wang and Sarker, 2006)
$T C_{r}=\frac{D}{Q_{f}} n_{o} K_{o}+\frac{Q_{f}}{2} \frac{H_{o}}{n_{o}}$


Fig. 6.9 Raw material inventory level in a multi-stage production system

### 6.3.1.2 Cost of work-in-process inventory

The production rate at the $i^{\text {th }}$ production system is carried at the rate of $\mathrm{P}_{\mathrm{i}}$. Since the semifinished products are shipped in batches, the number of kanbans are $\mathrm{K}_{\mathrm{i}}$, or the batch size is $\mathrm{Q}_{\mathrm{f}} / \mathrm{m}_{\mathrm{i}}$. The level of work-in-process inventory at the $\mathrm{i}^{\text {th }}$ production system is shown in Fig. 6.10. The cost of work-in-process inventory is written as (Wang and Sarker, 2006)

$$
\begin{equation*}
T C_{w i}=\frac{D}{Q_{f}}\left[m_{i} K_{i o}+K_{i s}\right]+\frac{Q_{f}}{2}\left[H_{i}\left(1-\frac{D}{P_{i}}\right)+\frac{H_{i}}{m_{i}}\right] \tag{6.49}
\end{equation*}
$$



Fig. 6.10 Work-in-process inventory of an intermediate stage

### 6.3.1.3 Cost of finished goods inventory

The total cost of the finished goods inventory in the last stage $\left(\mathrm{N}+1^{\text {th }}\right.$ stage) of the production system can be written as (Wang and Sarker, 2006)
$T C_{f}=\frac{D}{Q_{f}}\left[m_{N+1} K_{N+1, o}+K_{N+1, s}\right]+\frac{Q_{f}}{2}\left[H_{N+1}\left(1-\frac{D}{P_{N+1}}\right)+\frac{H_{N+1}}{m_{N+1}}\right]$

### 6.3.1.4 Total cost of multi-stage production system

The total cost of multi-stage production-delivery system consists of (i) the cost of raw materials at the first stage, (ii) the cost of WIP in the intermediate stages, and (iii) cost of finished goods at the last stage, can be written as

$$
\begin{align*}
& T C\left(Q_{f}, n_{1}, m_{1}, \ldots ., m_{N+1}\right)=\frac{D}{Q_{f}}\left[n_{o} K_{o}+\sum_{i=1}^{N+1} m_{i} K_{i o}+\sum_{i=1}^{N+1} K_{i s}\right] \\
& +\frac{Q_{f}}{2}\left[\frac{H_{o}}{n_{o}}+\sum_{i=1}^{N+1}\left\{H_{i}\left(1-\frac{D}{P_{i}}\right)+\frac{H_{i}}{m_{i}}\right\}\right] \tag{6.51}
\end{align*}
$$

### 6.3.1.5 Total cost of multi-stage production system with rework processing cost

Considering the rework processing cost, the total cost of multi-stage production-delivery system in Eq. (6.51) is written as
$T C=\frac{D K_{o}}{Q_{o}}+I_{o} H_{o}+\sum_{i=1}^{N+1} \frac{D K_{i o}}{Q_{i o}}+\sum_{i=1}^{N+1} \frac{D K_{i s}}{Q_{i}}+\sum_{i=1}^{N+1} D \beta_{i} C_{i}+\sum_{i=1}^{N+1} Q_{\text {avg }, i} H_{i}$
Substituting $\quad I_{o}=\frac{Q_{o}}{2}, \quad Q_{o}=\frac{Q_{r}}{n_{o}}, \quad Q_{i o}=\frac{Q_{i}}{m_{i}} \quad Q_{f}=Q_{i}=m_{i} x_{i}, \quad f=\frac{Q_{f}}{Q_{r}}, \quad \frac{D_{r}}{Q_{r}}=\frac{D_{i}}{Q_{i}}$ and $Q_{\text {avg }, i}=\frac{Q_{i}}{2}\left\{\left(1-\frac{D_{i}\left(1+\beta_{i}-\beta_{i}^{2}\right)}{P_{i}}\right)+\frac{1}{m_{i}}\right\}$

The expression for the total cost in Eq. (6.52) is obtained as

$$
\begin{align*}
& T C\left(Q_{f}, n_{o}, m_{1}, \ldots ., m_{N+1}\right)=\frac{D n_{o} f K_{o}}{Q_{f}}+\frac{Q_{f} H_{o}}{2 f n_{o}}+\sum_{i=1}^{N+1} \frac{D m_{i} K_{i o}}{Q_{f}}+\sum_{i=1}^{N+1} \frac{D K_{i s}}{Q_{f}} \\
& +\sum_{i=1}^{N+1} D \beta_{i} C_{i}+\sum_{i=1}^{N+1} \frac{Q_{i}}{2} H_{i}\left(1-\frac{D\left(1+\beta_{i}-\beta_{i}^{2}\right)}{P_{i}}\right)+\sum_{i=1}^{N+1} \frac{Q_{i}}{2} \frac{H_{i}}{m_{i}} \tag{6.53}
\end{align*}
$$

Considering $f=1$. the total cost expression in Eq. (6.53) is modified as

$$
\begin{align*}
& T C\left(Q_{f}, n_{o}, m_{1}, \ldots ., m_{N+1}\right)=\frac{D}{Q_{f}}\left[n_{o} K_{o}+\sum_{i=1}^{N+1} m_{i} K_{i o}+\sum_{i=1}^{N+1} K_{i s}\right]+\sum_{i=1}^{N+1} D \beta_{i} C_{i}  \tag{6.54}\\
& +\frac{Q_{f}}{2}\left[\frac{H_{o}}{n_{o}}+\sum_{i=1}^{N+1} H_{i}\left(1-\frac{D\left(1+\beta_{i}-\beta_{i}^{2}\right)}{P_{i}}\right)+\sum_{i=1}^{N+1} \frac{H_{i}}{m_{i}}\right]
\end{align*}
$$

If the integer restriction is not considered, the partial derivatives with respect to $n_{o}, m_{1}, m_{2}, \ldots$, $m_{N+l}$, (where $n_{o}, m_{l}, m_{2}, \ldots, m_{N+l} \geq 1$ and an integer) leads to

$$
\begin{equation*}
n_{o}^{*}=Q_{f} \sqrt{\frac{H_{o}}{2 D K_{o}}} \text { and } m_{i}^{*}=Q_{f} \sqrt{\frac{H_{i}}{2 D K_{i o}}} \tag{6.55}
\end{equation*}
$$

Substituting the optimal values of $\mathrm{n}_{\mathrm{o}}, \mathrm{m}_{1}, \mathrm{~m}_{2}, \ldots, \mathrm{~m}_{\mathrm{N}+1}$ from Eq. (6.55) in Eq. (6.54), leads to

$$
\begin{align*}
& T C\left(Q_{f}, n_{o}, m_{1}, \ldots ., m_{N+1}\right)=\sqrt{2 D H_{o} K_{o}}+\sum_{i=1}^{N+1} \sqrt{2 D H_{i} K_{i o}}+\frac{1}{Q_{f}} \sum_{i=1}^{N+1} D K_{i s}+\sum_{i=1}^{N+1} D \beta_{i} C_{i} \\
& +Q_{f} \sum_{i=1}^{N+1}\left\{\frac{H_{i}}{2}\left(1-\frac{D\left(1+\beta_{i}-\beta_{i}^{2}\right)}{P_{i}}\right)\right\} \tag{6.56}
\end{align*}
$$

The optimal production batch size $Q_{f}$ is given by

$$
\begin{equation*}
Q_{f}^{*}=\sqrt{\frac{2 D \sum_{i=1}^{N+1} K_{i s}}{\sum_{i=1}^{N+1}\left\{H_{i}\left(1-\frac{D_{i}\left(1+\beta_{i}-\beta_{i}^{2}\right)}{P_{i}}\right)\right\}}} \tag{6.57}
\end{equation*}
$$

Substituting the optimal value of production batch size Q from Eq. (6.57) in Eq. (6.56), leads to

$$
\begin{align*}
& T C\left(Q_{f}, n_{o}, m_{1}, \ldots ., m_{N+1}\right)=\sqrt{2 D H_{o} K_{o}}+\sum_{i=1}^{N+1} \sqrt{2 D H_{i} K_{i o}} \\
& +\sqrt{2 D} \sqrt{\sum_{i=1}^{N+1}\left\{H_{i}\left(1-\frac{D_{i}\left(1+\beta_{i}-\beta_{i}^{2}\right)}{P_{i}}\right)\right\} \sqrt{\sum_{i=1}^{N+1} K_{i s}}+D \sum_{i=1}^{N+1} \beta_{i} C_{i}} \tag{6.58}
\end{align*}
$$

### 6.3.2 Computational results

Assume that the proportion of defective items $\left(\beta_{i}\right)$ in all stages is 0.01 and the rework processing cost $\left(C_{i}\right)$ in all stages is $\$ 10.0$. Table 6.13 shows the input data for a multi-stage production system under kanban mechanism (Wang and Sarker, 2006). The comparison of optimal and modified results for a multi-stage production system under kanban mechanism with rework consideration are shown in Table 6.14. The optimal results of $n_{0}, m_{l}, \ldots ., m_{4}, Q_{f}, T C$ show an increase with rework consideration. The modified results of $n_{0}, m_{1}, \ldots, m_{4}, Q_{f}$ are similar for with and without rework except in $m_{4}$ which shows an increase with rework consideration. The total cost for optimal and modified results increase with rework due to the rework processing cost consideration. Table 6.15 shows a comparison of all possible combinations of modified results for a multi-stage production system under kanban mechanism with rework consideration.

Figures 6.11 and 6.12 show the total cost (TC) increases with increase in proportion of defective items $\left(\beta_{\mathrm{i}}\right)$ and rework processing cost $\left(\mathrm{C}_{\mathrm{i}}\right)$ respectively. Figure 6.13 shows the variation of total $\operatorname{cost}(\mathrm{TC})$ with both proportion of defective items $\left(\beta_{\mathrm{i}}\right)$ and rework processing cost $\left(\mathrm{C}_{\mathrm{i}}\right)$. Total cost (TC) increases with increase in both $\beta_{\mathrm{i}}$ and $\mathrm{C}_{\mathrm{i}}$ respectively. The increase in total cost (TC) with $C_{i}$ is more at higher values of $\beta_{i}$.


Fig. 6.11 Variation of TC with $\boldsymbol{\beta}_{\mathrm{i}}$


Fig. 6.12 Variation of $\mathbf{T C}$ with $\mathbf{C}_{\mathbf{i}}$


Fig. 6.13 Variation of TC with $\boldsymbol{\beta}_{i}$ and $C_{i}$

Table 6.13 Input data for a multi-stage production system under kanban mechanism

$$
\left(K_{o}=110, H_{o}=45, \beta_{i}=0.01, C_{i}=10(i=1,2,3,4)\right)
$$

| Demand of <br> finished goods <br> (units/year) | Production rate <br> (units/year) | Setup/shipping cost <br> (\$/batch) | Setup cost <br> (\$/batch) | Holding cost <br> (\$/unit/year) |
| :--- | :--- | :--- | :--- | :--- |
| $=50000$ | $P_{1}=5500$ | $K_{l s}=300$ | $K_{1 o}=100$ | $H_{l}=30$ |
|  | $P_{2}=5600$ | $K_{2 s}=250$ | $K_{2 o}=80$ | $H_{2}=45$ |
|  | $P_{3}=6000$ | $K_{3 s}=300$ | $K_{3 o}=120$ | $H_{3}=25$ |
|  | $P_{4}=5500$ | $K_{4 s}=350$ | $K_{4 o}=100$ | $H_{4}=35$ |

Table 6.14 Comparison of results for a multi-stage production system under kanban mechanism

|  | Wang and Sarker $(2006)$ |  | Present work (with rework consideration) |  |
| :--- | :--- | :--- | :--- | :--- |
|  | Optimum results | Modified results | Optimum results | Modified results |
| $n_{0}$ | 5.74 | 6 | 5.98 | 6 |
| $m_{l}$ | 4.92 | 5 | 5.12 | 5 |
| $m_{2}$ | 6.73 | 7 | 7.02 | 7 |
| $m_{3}$ | 4.10 | 4 | 4.27 | 4 |
| $m_{4}$ | 5.31 | 5 | 5.54 | 6 |
| $Q_{f}$ | 898 | 898 | 936 | 936 |
| TC $(\$)$ | 43277 | 43301 | 44732 | 44765 |

Table 6.15 Comparison of all possible modified results for a multi-stage production system under kanban mechanism

| S. | Wang and Sarker (2006) |  |  |  |  |  |  | Present work (with rework consideration) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | $n_{0}$ | $m_{1}$ | $m_{2}$ | $m_{3}$ | $m_{4}$ | $Q_{f}$ | TC (\$) | $n_{0}$ | $m_{1}$ | $m_{2}$ | $m_{3}$ | $m_{4}$ | $Q_{f}$ | TC (\$) |
| 1 | 5.0 | 4.0 | 6.0 | 4.0 | 5.0 | 897.5 | 43512.5 | 5.0 | 5.0 | 7.0 | 4.0 | 5.0 | 935.6 | 44889.8 |
| 2 | 5.0 | 4.0 | 6.0 | 4.0 | 6.0 | 897.5 | 43546.1 | 5.0 | 5.0 | 7.0 | 4.0 | 6.0 | 935.6 | 44878.4 |
| 3 | 5.0 | 4.0 | 6.0 | 5.0 | 5.0 | 897.5 | 43620.1 | 5.0 | 5.0 | 7.0 | 5.0 | 5.0 | 935.6 | 44946.3 |
| 4 | 5.0 | 4.0 | 6.0 | 5.0 | 6.0 | 897.5 | 43653.6 | 5.0 | 5.0 | 7.0 | 5.0 | 6.0 | 935.6 | 44934.9 |
| 5 | 5.0 | 4.0 | 7.0 | 4.0 | 5.0 | 897.5 | 43477.4 | 5.0 | 5.0 | 8.0 | 4.0 | 5.0 | 935.6 | 44941.4 |
| 6 | 5.0 | 4.0 | 7.0 | 4.0 | 6.0 | 897.5 | 43510.9 | 5.0 | 5.0 | 8.0 | 4.0 | 6.0 | 935.6 | 44930.0 |
| 7 | 5.0 | 4.0 | 7.0 | 5.0 | 5.0 | 897.5 | 43584.9 | 5.0 | 5.0 | 8.0 | 5.0 | 5.0 | 935.6 | 44997.9 |
| 8 | 5.0 | 4.0 | 7.0 | 5.0 | 6.0 | 897.5 | 43618.5 | 5.0 | 5.0 | 8.0 | 5.0 | 6.0 | 935.6 | 44986.5 |
| 9 | 5.0 | 5.0 | 6.0 | 4.0 | 5.0 | 897.5 | 43396.5 | 5.0 | 6.0 | 7.0 | 4.0 | 5.0 | 935.6 | 44956.3 |
| 10 | 5.0 | 5.0 | 6.0 | 4.0 | 6.0 | 897.5 | 43430.0 | 5.0 | 6.0 | 7.0 | 4.0 | 6.0 | 935.6 | 44945.0 |
| 11 | 5.0 | 5.0 | 6.0 | 5.0 | 5.0 | 897.5 | 43504.0 | 5.0 | 6.0 | 7.0 | 5.0 | 5.0 | 935.6 | 45012.9 |
| 12 | 5.0 | 5.0 | 6.0 | 5.0 | 6.0 | 897.5 | 43537.6 | 5.0 | 6.0 | 7.0 | 5.0 | 6.0 | 935.6 | 45001.5 |
| 13 | 5.0 | 5.0 | 7.0 | 4.0 | 5.0 | 897.5 | 43361.3 | 5.0 | 6.0 | 8.0 | 4.0 | 5.0 | 935.6 | 45008.0 |
| 14 | 5.0 | 5.0 | 7.0 | 4.0 | 6.0 | 897.5 | 43394.9 | 5.0 | 6.0 | 8.0 | 4.0 | 6.0 | 935.6 | 44996.6 |
| 15 | 5.0 | 5.0 | 7.0 | 5.0 | 5.0 | 897.5 | 43468.9 | 5.0 | 6.0 | 8.0 | 5.0 | 5.0 | 935.6 | 45064.5 |
| 16 | 5.0 | 5.0 | 7.0 | 5.0 | 6.0 | 897.5 | 43502.5 | 5.0 | 6.0 | 8.0 | 5.0 | 6.0 | 935.6 | 45053.1 |
| 17 | 6.0 | 4.0 | 6.0 | 4.0 | 5.0 | 897.5 | 43452.2 | 6.0 | 5.0 | 7.0 | 4.0 | 5.0 | 935.6 | 44775.9 |
| 18 | 6.0 | 4.0 | 6.0 | 4.0 | 6.0 | 897.5 | 43485.7 | 6.0 | 5.0 | 7.0 | 4.0 | 6.0 | 935.6 | 44764.5 |
| 19 | 6.0 | 4.0 | 6.0 | 5.0 | 5.0 | 897.5 | 43559.8 | 6.0 | 5.0 | 7.0 | 5.0 | 5.0 | 935.6 | 44832.4 |
| 20 | 6.0 | 4.0 | 6.0 | 5.0 | 6.0 | 897.5 | 43593.3 | 6.0 | 5.0 | 7.0 | 5.0 | 6.0 | 935.6 | 44821.0 |
| 21 | 6.0 | 4.0 | 7.0 | 4.0 | 5.0 | 897.5 | 43417.0 | 6.0 | 5.0 | 8.0 | 4.0 | 5.0 | 935.6 | 44827.5 |
| 22 | 6.0 | 4.0 | 7.0 | 4.0 | 6.0 | 897.5 | 43450.6 | 6.0 | 5.0 | 8.0 | 4.0 | 6.0 | 935.6 | 44816.1 |
| 23 | 6.0 | 4.0 | 7.0 | 5.0 | 5.0 | 897.5 | 43524.6 | 6.0 | 5.0 | 8.0 | 5.0 | 5.0 | 935.6 | 44884.0 |
| 24 | 6.0 | 4.0 | 7.0 | 5.0 | 6.0 | 897.5 | 43558.2 | 6.0 | 5.0 | 8.0 | 5.0 | 6.0 | 935.6 | 44872.6 |
| 25 | 6.0 | 5.0 | 6.0 | 4.0 | 5.0 | 897.5 | 43336.1 | 6.0 | 6.0 | 7.0 | 4.0 | 5.0 | 935.6 | 44842.5 |
| 26 | 6.0 | 5.0 | 6.0 | 4.0 | 6.0 | 897.5 | 43369.7 | 6.0 | 6.0 | 7.0 | 4.0 | 6.0 | 935.6 | 44831.1 |
| 27 | 6.0 | 5.0 | 6.0 | 5.0 | 5.0 | 897.5 | 43443.7 | 6.0 | 6.0 | 7.0 | 5.0 | 5.0 | 935.6 | 44899.0 |
| 28 | 6.0 | 5.0 | 6.0 | 5.0 | 6.0 | 897.5 | 43477.3 | 6.0 | 6.0 | 7.0 | 5.0 | 6.0 | 935.6 | 44887.6 |
| 29 | 6.0 | 5.0 | 7.0 | 4.0 | 5.0 | 897.5 | 43301.0 | 6.0 | 6.0 | 8.0 | 4.0 | 5.0 | 935.6 | 44894.1 |
| 30 | 6.0 | 5.0 | 7.0 | 4.0 | 6.0 | 897.5 | 43334.6 | 6.0 | 6.0 | 8.0 | 4.0 | 6.0 | 935.6 | 44882.7 |
| 31 | 6.0 | 5.0 | 7.0 | 5.0 | 5.0 | 897.5 | 43408.6 | 6.0 | 6.0 | 8.0 | 5.0 | 5.0 | 935.6 | 44950.6 |
| 32 | 6.0 | 5.0 | 7.0 | 5.0 | 6.0 | 897.5 | 43442.1 | 6.0 | 6.0 | 8.0 | 5.0 | 6.0 | 935.6 | 44939.2 |

### 6.4 Managerial Implications

The managerial implications are as follows:

- For single purchase multiple delivery (SPMD), single purchase single delivery (SPSD), and for lot-for-lot (LFL) policies, with increase in the fraction of non-conforming units $(\alpha)$, and value added by the manufacturing process (V), the (i) optimal number of inspections increases, (ii) optimal ordering quantity decreases, and (iii) optimal expected total cost increases. As shown in Table 6.2 for imperfect production process with quality and rework of SPMD policy, with increase in the fraction of non-conforming units ( $\alpha$ ) from 0.05 to 0.50 , the (i) optimal ordering quantity decreased from 274 to 126 , and (ii) optimal expected total cost increased from $\$ 3512.78$ to $\$ 4438.64$. As shown in Table 6.3 for imperfect production process with quality and rework including process inspection and restoration of SPMD policy, with increase in the fraction of non-conforming units ( $\alpha$ ) from 0.05 to 0.50 , the (i) optimal number of inspections increased from 3 to 5, (ii) optimal ordering quantity decreased from 316 to 147, and (iii) optimal expected total cost increased from $\$ 3496.45$ to $\$ 4031.10$. As shown in Table 6.2 for imperfect production process with quality and rework of SPMD policy, with increase in the value added by the manufacturing process (V) from 1.0 to 8.0 , the (i) optimal ordering quantity decreased from 274 to 126 , and (ii) optimal expected total cost increased from $\$ 3512.78$ to $\$$ 20593.97. As shown in Table 6.3 for imperfect production process with quality and rework including process inspection and restoration of SPMD policy, with increase in the value added by the manufacturing process (V) from 1.0 to 8.0 , the (i) optimal number of inspections increased from 3 to 4, (ii) optimal ordering quantity decreased from 316 to 147, and (iii) optimal expected total cost increased from \$ 3496.45 to \$ 20593.97.
- In the model of optimal batch size in a single-stage imperfect production-delivery system with rework, wherein defective items are reworked within the same cycle, the total cost increase with defects due to rework processing cost consideration to compensate for the loss of planned products. As shown in Table 6.12 (S. No.1), the total cost with rework consideration is $\$ 1323$, while the total cost without rework consideration (Sarker and Parija, 1996) is $\$ 1206$. Also, in the model of optimal number of kanbans for multi-stage production-delivery system with rework, wherein defective items are reworked within the same cycle, the optimal quantity and total cost increase with defects due to rework
processing cost consideration. As shown in Table 6.14, the optimal quantity and total cost with rework consideration are 936 and $\$ 44765$, while the optimal quantity and total cost without rework consideration (Wang and Sarker, 2006) are 898 and $\$ 43301$.

